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# **MONITORING WELL INSTALLATION , SAMPLING AND ANALYSIS**

**for**

**SECO Products**

**Washington, Missouri**

**February, 1983**



R00348970  
RCRA RECORDS CENTER



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## TABLE OF CONTENTS

	<u>Page No.</u>
Title Page	i
Table of Contents	ii
List of Tables	iii
List of Figures	iii

### Chapter No.

1	INTRODUCTION	1
2	FIELD INVESTIGATIONS Well Drilling and Installation Well Development- Surveying Monitoring Well Sampling Aquifer Testing	2
3	GEOLOGY AND SOILS	9
4	GROUNDWATER Groundwater Flow Direction and Rate Groundwater Quality	11

### APPENDICES:

Appendix A:	Field Boring Logs
Appendix B:	Well Construction Details
Appendix C:	Aquifer Testing
Appendix D:	<i>First years sampling results &amp; water table elevations</i>

## LIST OF TABLES

<u>Table No.</u>		<u>Page No.</u>
1	Well Construction Data	5
2	Statistical Representation of Background Monitoring Well No. 2	6
3	Summary of Aquifer Test Results	7
4	Results of Analyses	13

## LIST OF FIGURES

<u>Figure No.</u>		
1	SECO-Monitoring Well Locations	3
2	General Soil Cross-Section Around Waste Lagoon	10

## CHAPTER 1

### INTRODUCTION

In order to comply with the current regulations promulgated by both the U. S. Environmental Protection Agency (USEPA) and the Missouri Department of Natural Resources (MO DNR) in response to the Resource Conservation and Recovery Act (RCRA) P.O. 94-580, SECO Products retained Envirodyne Engineers, Inc. (Envirodyne), acting as a subcontractor to Theiss Engineers, Inc. to supervise the installation of and sample a monitoring well network around SECO's industrial wastewater lagoon. Six monitoring wells were installed by Wabash Drilling, Inc. under Envirodyne's supervision from September 22-27, 1982. Well locations and elevations were surveyed by Envirodyne and Theiss Engineers personnel on October 4, 1982, at which time water level elevations were also measured. Two rounds of water samples were collected and analyzed by Envirodyne. These samples were collected on October 5 and November 2, 1982.

This report documents the field activities which were conducted, and describes the soils encountered during the installation of the wells. The results of the aquifer tests which Envirodyne conducted on the wells and the chemical analysis results are also included in this report. Well logs, well construction details and aquifer test data are included as Appendices A, B and C, respectively.

## CHAPTER 2

### FIELD INVESTIGATIONS

#### WELL DRILLING AND INSTALLATION

The borings were advanced using hollow stem augers (HSA), 4-inch I.D. (nominal). Split spoon samples were collected continuously at wells 1, 3 and 4 (Figure 1). At wells 2, 5 and 6, split spoon samples were collected at 2-1/2 foot intervals. The soils encountered were described and visually classified in the field. These descriptions and classifications are shown in the logs in Appendix A.

During drilling and sampling the "first encountered water" depth was noted, and the boring advanced approximately 15 feet deeper than that point. The center plug was removed and the 2-1/2 inch diameter well screen and pipe were placed inside the hollow stem of the auger. The sand backfill and bentonite seal were then placed as the augers were backed out of the hole from around the well. The cement grout was emplaced above the bentonite seal to ground surface. A six inch steel protector pipe was emplaced at Well #6.

The well screen and well pipe are 2-1/2 inch diameter Sch. 40 PVC, box-threaded. The well screens are each 15 feet long and commercially slotted with 0.006 inch wide slots. Coarse filter sand was used as backfill material around the well screens. Bentonite pellets were used to create a bentonite seal. The grout was a cement/bentonite mix with a volume ratio of 6:1, cement/bentonite.

#### WELL DEVELOPMENT

The wells were developed using a 1-1/4 inch diameter, 10 feet long bailer. An initial attempt was made to bail the wells until clear. It became evident that due to the fine-grained nature of the soils encountered, no reasonable amount of activity would achieve clear water. A total of 40 gallons of water was removed from each well over a period of two days.

#### SURVEYING

The monitoring wells were located with the use of a transit and steel tape. Elevations were determined from a U.S.G.S. monument located on the northeast corner of the railroad bridge which crosses Dubois Creek. The elevation of the standpipe

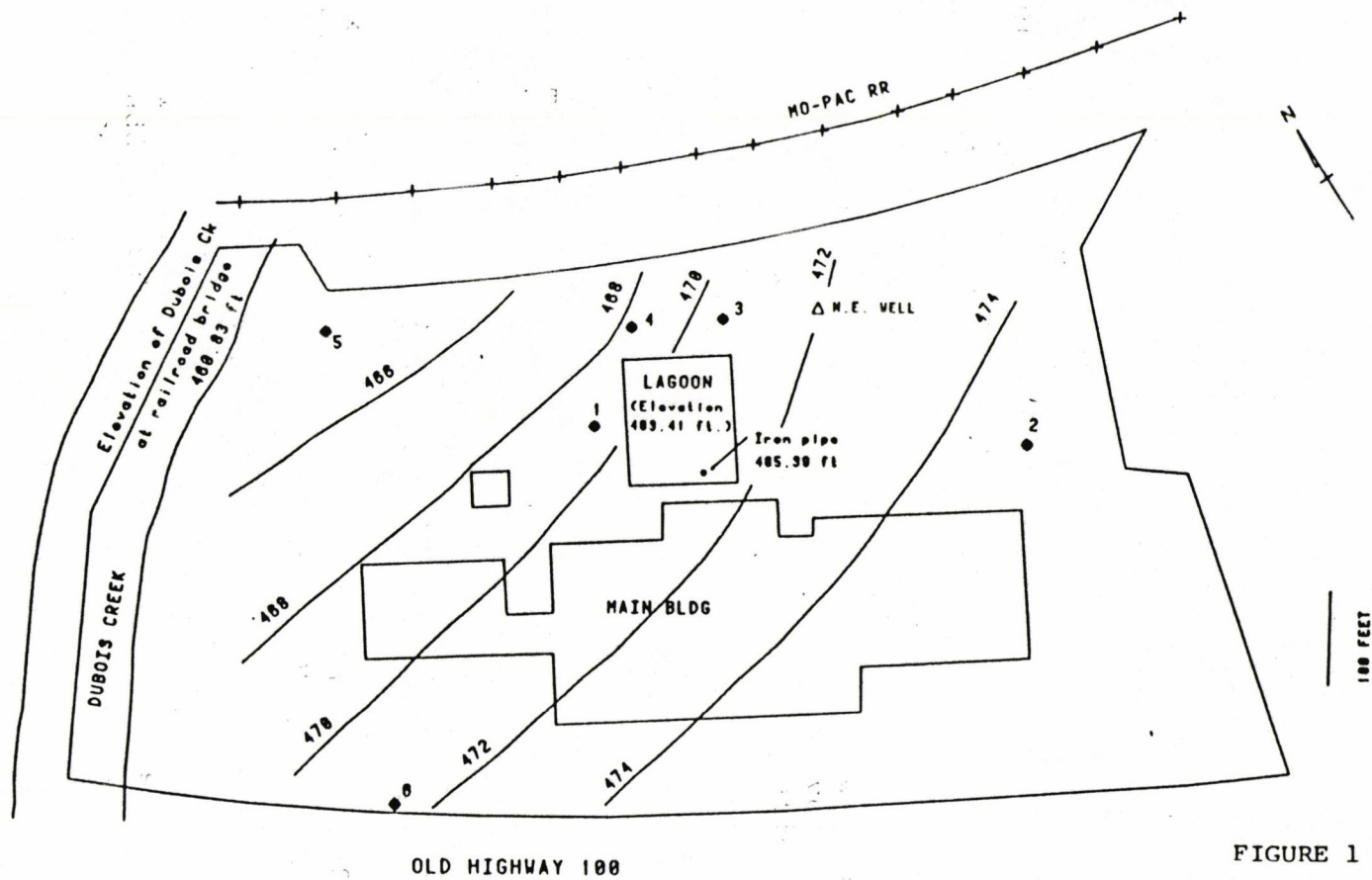


FIGURE 1  
SECO - MONITORING WELL LOCATIONS

- MONITORING WELL
  - △ EXISTING WELL
  - + RAILROAD
- Groundwater elevations  
Measured on 10/4/82  
Groundwater contours in ft

EEI



was measured at each well with the use of a level and stadia rod. Other measurements at each site included depth to water from top of the well pipe (taken at highest edge), depth to bottom of well, and height of well pipe above ground. (Table 1)

#### MONITORING WELL SAMPLING

Upon completion of drilling, development and surveying, the new wells were allowed to set for six days before sampling. Four wells were selected for sampling (3 down gradient wells from the waste lagoon and one up gradient well). Equipment used in the sampling included an 8 foot by 1-1/4 inch PVC well-bailer lowered with a nylon cord. A fiberglass tape measure with a steel popper was used to determine the water table depth. Each well was purged by removing 10 gallons of water with the bailer. A sample was then taken from the well with the bailer and placed in the appropriate containers. A portion of the sample was filtered through a .45  $\mu$ m filter and then preserved with nitric acid for metal analysis. Electrical conductivity and pH were measured in the field. At Well #2 (Background well) electrical conductivity and pH were measured four times during a 2 hour period (Table 2). All the samples were placed in a cooler and iced for cold preservation and driven back to St. Louis that evening and placed in refrigeration until analyzed.

#### AQUIFER TESTING

Slug tests were performed by EEI personnel on the six monitoring wells. The field procedure consisted of rapidly lowering a solid slug of known volume to the bottom of the well, causing an essentially instantaneous rise in the water level in the well. The rate at which the water level returned to equilibrium was then measured and recorded. The slug consisted of a sealed section of PVC pipe filled with a mixture of sand and water. No external fittings were used on the pipe so that 1-1/4 inch pipe could be used without restricting the flow of water within the annulus between the slug and the inside wall of the 2-1/2 inch (nominal) well pipe/screen.

The water level recovery was measured with a fiberglass tape measure with a bell-shaped pipe fitting on the end. The pipe fitting added weight and produced a popping sound when striking the surface of the water. This system enabled reasonably accurate and precise water level measurements to be made fairly quickly. The data from these tests are included in Table 3 and Appendix C.

TABLE 1  
WELL CONSTRUCTION DATA

<u>Well Number</u>	<u>Well Depth (Feet Below Ground Surface)</u>	<u>Top of Casing (TOC) Elevation (Feet)</u>	<u>Stick-Up (Feet)</u>	<u>Groundwater Elevation (Feet)</u>	<u>Date</u>	<u>Ground Elevation (Feet)</u>
1	23.3	482.01	1.7	469.48	10/4/82	480.3
2	32.9	494.90	2.1	475.14	10/4/82	492.8
3	22.5	482.75	2.5	470.47	10/4/82	480.3
4	22.4	481.82	2.6	468.84	10/4/82	479.2
5	26.8	484.19	3.2	464.86	10/4/82	481.0
6	38.4	493.35	1.6	471.53	10/4/82	491.8

Elevation of waste lagoon - 483.41  
Elevation of iron pipe in waste lagoon - 485.39  
Elevation of Dubois Creek at Railroad Bridge - 460.83

TABLE 2  
STATISTICAL REPRESENTATION OF BACKGROUND MONITORING WELL #2

<u>Parameter</u>	<u>Rep. 1</u>	<u>Rep. 2</u>	<u>Rep. 3</u>	<u>Rep. 4</u>	<u>Mean</u>	<u>Variance</u>
pH (units)	6.7	6.6	6.6	6.7	6.65	0.003
specific conductance (μmhos)	600	600	575	600	593.75	156.25
TOC mg/l	14	20	16	13	15.75	9.58
TOH, μg/l as Cl <sup>-</sup>	14	6	≤5	≤5	7.5	19.00

9

10/4/82

TABLE 3  
SUMMARY OF AQUIFER TEST RESULTS

Well No.	Horizontal Coefficient of Permeability cm/sec	i Water Table Gradient	V Horizontal (a) Flow Rate		Potential Historic Extent of Migration (b)	
			m/yr	ft/yr	m	ft
1	$6.7 \times 10^{-4}$	0.0222	13.4	44.1	94	309
2	$3.3 \times 10^{-3}$	0.0133	40.1	131.2	281	918
3	$1.8 \times 10^{-3}$	0.0156	25.8	84.7	181	593
4	$2.1 \times 10^{-3}$	0.0303	57.3	188.0	401	1316
5	$1.3 \times 10^{-2}$	0.0199	228.1	748.2	1597	5237
6	$4.7 \times 10^{-3}$	0.0154	65.2	213.8	456	1497

(a)  $V = \frac{Ki}{n}$

n = porosity assumed at 0.35  
K + i as described above

(b) based on 7 year existence of lagoon

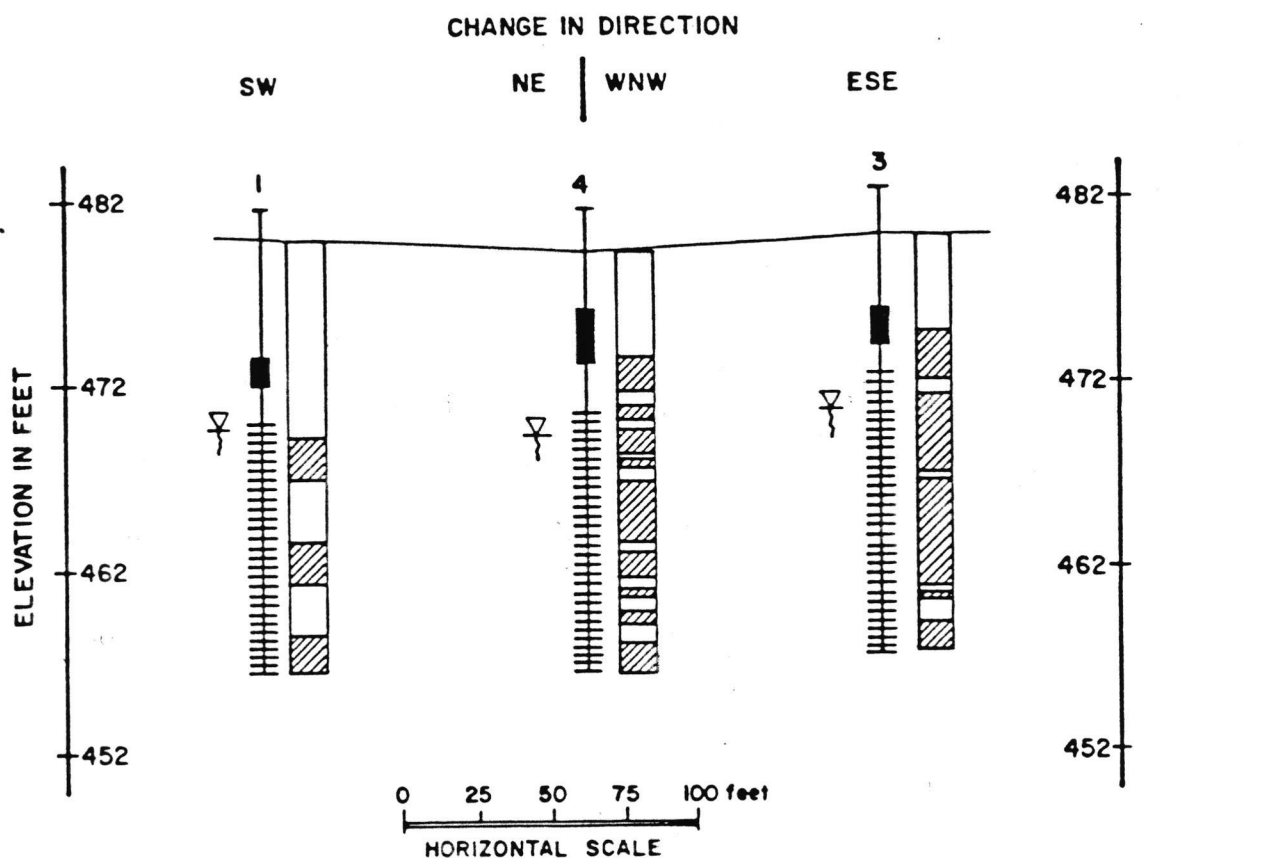
The recovery data was analyzed using the curve matching technique described by Papadopoulos (1967). Since the aquifer in most instances is not confined, and the wells used for the tests were not fully penetrating (assumptions for this method), the results obtained (shown in Appendix A) are not extremely accurate. However, they do indicate the coefficient of permeability of the soils surrounding the screens of the wells tested to within a plus or minus order of magnitude. Table 3 is a summary of the results obtained from aquifer testing. The aquifer testing measured the coefficient of permeability (K), which when coupled with the water table gradient (i) and the estimated porosity (n), can be used to determine the horizontal flow rate (V) using the relation  $V = Ki/n$ . In this manner, a flow rate is calculated which can be used in estimating theoretical contaminant migration rates.



### CHAPTER 3

#### GEOLOGY AND SOILS

The six soil borings indicated the presence of stratified fluvially deposited material. The soil texture is very heterogeneous both laterally and vertically. Stratified coarse and fine textured soils throughout the borings were very common with the exception of boring #6 which contained fine-grained soils down to 34 feet.

In general, the cross-section (see Figure 2) encompassing the three wells close to the waste lagoon indicated that the uppermost soils are fine grained (silt loams, silty clay loams, and clay loams). Borings 3 & 4 located on the northeast side of the lagoon contained generally fine grained soils down to approximately 5 feet. Below 5' stratified coarse and fine grained soils occur throughout the total depth of the borehole (=23 feet). Boring #1 on the northwest side of the lagoon contained fine textured soils down to eleven feet. Below 11 feet, stratified coarse and fine grained soil occurs, however, the stratification is not as prevalent as in borings 4 & 3. Boring #5 located near the northwest corner of the property contained fine textured soils down to 8'. Below 8', stratified coarse and fine textured soils occurred down to 22.5' at which point coarse sand and gravel were encountered throughout the remaining depth of the borehole (29 feet).



-  Very rapid Permeability (Sand, Loamy Sand, and Sandy Loam)
-  Relatively Impermeable (Siltloam, Sandy clay loam, Clay loam, Silty clay loam, Sandy clay and Silty clay)

NOTE:

Groundwater elevations were measured on 10-4-82.  
 Elevation of waste lagoon 483.41.  
 Elevation of Dubois Creek at RR Bridge 460.83

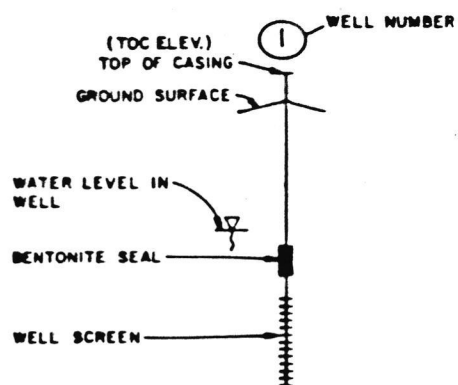


FIGURE 2

GENERAL SOIL CROSS-SECTION  
 AROUND WASTE LAGOON

EEI



## CHAPTER 4

### GROUNDWATER

#### GROUNDWATER FLOW DIRECTION AND RATE

Due to the proximity of the waste lagoon to Dubois Creek and the Missouri River, the water table configuration here is highly variable. Periods of flooding and low water can cause reversals of the groundwater flow direction, and change the rate of migration of any possible transported contaminants. Water table measurements were made during the aquifer testing under conditions which were assumed to be normal flow conditions.

At the time of measuring, the groundwater flow direction was in a northwesterly direction with the ultimate discharge into Dubois Creek. Figure 1 is a representation of the water table at this time, based upon the water levels in the six monitoring wells shown. The groundwater flows toward Dubois Creek with a horizontal flow rate varying from 44/ft/yr to 748 ft/yr, as shown in Table 3. The water table gradient in this area ranges from a high of 0.0303 (3.03%) to a low value of 0.0133 (1.33%). A typical value for the coefficient of permeability of the more permeable strata at SECO is about  $3.4 \times 10^{-3}$  cm/sec. With an effective porosity of .35 assumed for this permeable sandy strata and a range of water table gradients of 0.0133 to 0.0303, the resultant groundwater flow rates range from 41 m/yr (134 ft/yr) to 93 m/yr (305 ft/yr). Well #5, closest to the creek, had a horizontal flow rate of 748 feet per year. Inspection of the boring logs revealed a fairly deep sand and gravel layer within the lower seven feet of the well screen. The high flow rate here can be attributed to this gravel layer.

#### DETERMINATION OF PROPER WELL PLACEMENT

Using the average flow rate range of 41 to 93 m/yr, any possible contamination from the lagoon could have traveled from 278 m to 651 meters (941 to 2135 feet). These distances are based on the 7 year existence of the lagoon, and assume that contaminants entered the flow system when the lagoon was first put into operation. At these rates, all the down gradient wells (Nos. 1, 3, 4, 5) are within the potential migration distance from the lagoon. The suspected reversal of the groundwater flow due to periodic flooding may reduce these distances somewhat, but these wells should still be within the theoretical contaminant migration distance. Therefore, these wells appear to be properly positioned for monitoring the lagoon.

#### GROUNDWATER QUALITY

The groundwater in the vicinity of the waste lagoon is of generally good quality (Table 4). The pH of the groundwater at Well #1 and Well #4 was 0.3 pH units below the background well #2 and 0.2 pH units lower than the recommended limit for drinking water (MO DNR). Monitoring wells #1 and #4 are downgradient and very close to the waste lagoon. It appears that some acid from the waste lagoon may have entered the aquifer, however, it appears equally probable that the slight decrease in pH is attributable to operations conducted prior to the construction of the lagoon. The specific conductance at Well #1 was slightly higher (900  $\mu$ mhos) than the background Well #2 (594  $\mu$ mhos), indicating a higher concentration of free salts in the groundwater.

The fecal coliform count in all the monitoring wells were above the state drinking water limit of 1 count/100 ml. Background Well #2 contained 300 counts/100 ml while Well #1, #4 and #5 had 45 counts/100 ml or below. The reason for well #2 containing a higher count is unclear. One explanation may be due to the fact that the wells were not disinfected after installation. The counts shown may be a result of contamination introduced during drilling.

The remainder of the parameters (metals, organics, salts, and radioactivity) were all below the state and Federal standards.

10/5/82 &amp; 11/2/82

TABLE 4  
RESULTS OF ANALYSES

Parameters (a)	Well #1	Well #2	Well #4	Well #5	EPA and/or MO (c) Department of Natural Resources Standard
					6.5 - 9.0 (d)
pH (units)	6.3	6.65 (b)	6.3	7.0	--
specific conductance (umhos/cm)	900	593.75 (b)	550	450	--
TOC	<1	15.75 (b)	13	14	--
TOH (ug/l as Cl <sup>-</sup> )	14	7.5 (b)	33	68	
arsenic	0.009	0.002	0.009	<0.002	0.05
barium	<0.05	<0.05	<0.05	<0.05	1.0
cadmium	<0.001	<0.001	<0.001	<0.001	0.010
chromium	<0.003	<0.003	<0.003	<0.003	0.05
copper	0.011	0.007	0.004	0.003	10
iron	<0.04	<0.04	<0.04	<0.04	0.3
lead	0.003	0.003	0.003	0.002	0.05
manganese	0.06	0.10	0.04	0.04	0.05
mercury	<0.0002	<0.002	<0.002	<0.002	0.002
nickel	<0.04	<0.04	<0.14	<0.04	1.0 (d)
selenium	<0.002	<0.002	<0.002	<0.002	0.01
silver	<0.001	<0.001	<0.001	<0.001	0.05
sodium	16.2	10.3	16.8	5.14	--
zinc	0.028	0.079	0.025	0.031	1.0 (d)
chloride	10.2	10.4	4.9	2.1	250
cyanide	<0.005	<0.005	<0.005	<0.005	0.005 (d)
fluoride	0.43	0.39	0.19	0.72	2.2
phenols	0.008	0.007	0.007	0.006	0.001 (d)
sulfate	25	40	20	20	250
nitrate	8.10	0.35	5.00	4.65	10
fecal coliform (counts/100 ml)	45	300	5	5	1
lindane (ug/l)	<0.003	<0.003	<0.003	<0.003	4.0
endrin (ug/l)	<0.004	<0.004	<0.004	<0.004	0.2
methoxychlor (ug/l)	<0.05	<0.05	<0.05	<0.05	100
toxaphene (ug/l)	<0.2	<0.2	<0.2	<0.2	5
2,4-D (ug/l)	<0.005	<0.005	<0.005	<0.005	100
2,4,5-TP (ug/l)	<0.002	<0.002	<0.002	<0.002	10
Radioactive:	---	---	picocuries/Liter	---	---
Gross Alpha	16.1 ± 6.4	11.7 ± 5.0	7.17 ± 3.0	9.79 ± 3.7	15
Gross Beta	13.9 ± 3.1	13.7 ± 3.0	4.01 ± 2.4	8.11 ± 2.6	50
Radium, total	0.40 ± 0.29	0.37 ± 0.27	0.24 ± 0.23	0.36 ± 0.27	5
Radium - 226	0.54 ± 0.19	0.70 ± 0.21	0.25 ± 0.15	0.32 ± 0.16	--

(a) Values are mg/l except as noted.

(b) Value represents the mean of four replicates.

(c) Water Quality chart published by the St. Louis County Water Company, February 1981

(d) Missouri 10 CSR 20-7.031, as amended through March 19, 1982

APPENDIX A  
FIELD BORING LOGS





SECO Products

JOB NO 1735

BORING NO 1

LOCATION West of Lagoon Elev 480.3

GROUND WATER While drilling 8' Time after drilling \_\_\_\_\_  
Before casing removal \_\_\_\_\_ Depth to water \_\_\_\_\_  
After casing removal \_\_\_\_\_ Depth to cave-in \_\_\_\_\_  
Start \_\_\_\_\_  
Unit \_\_\_\_\_  
Chief \_\_\_\_\_

Sample No	Moisture	Blows on Sampler		Recovery	Penetration	VISUAL FIELD CLASSIFICATION AND REMARKS (Intervals are in feet)	S.S. Dia <u>2"</u> Weight <u>140 lbs</u> Drop <u>30"</u>	Pump Pressure	Boulders	Drilling fluid		Drilling Method	Graphic Log
		0/6	6/18							Fluid Type	Fluid Loss		
A		1	4			Very dark grayish brown (10yr3/2) light sandy clay loam (SC)							HS2
						10		10					
S		2	8										
						11		11					
S		2	5			12 Dark brown (10YR4/3) loamy sand (SM)		12					
						13		13					
S		2	6			14 Dark grayish brown (10YR4/2) silt loam (SC)		14					
						15 Dark grayish brown sandy clay loam (SC)		15					
S		2	5			16 Grayish brown (10yr5/2) clay loam to sandy clay loam 1/4" sand lenses common (SC or CL)		16					
S		1	6			17 Dark brown (10YR3/3) loamy sand (SM)		17					
						18 Dark brown (10YR3/3) sandy loam (SC)		18					

Sheet 3 of 3

BORING NO 1

LOCATION West of Lagoon

Elev. 480.3

While drilling \_\_\_\_\_ 8'

Time after drilling

**Before casing removal**

Depth to water.

After casing removal

Depth to cave-in

**Start.**

Unit \_\_\_\_\_

**Chief,**

Sample	Moisture	Blows on Sampler		Recovery	Penetration	VISUAL FIELD CLASSIFICATION AND REMARKS (Intervals are in feet)	S.S. Dia <u>2"</u>	Pump Pressure	Boulders	Drilling fluid		Drilling Method	Graphic Log
		0/6	6/18				Weight <u>140 lbs</u>			Drop <u>30 lbs</u>	Fluid Type		
		2	5										
9	S												
						Dark gray (2.5Y4/0) sandy clay loam to loam (SC)							
						19	19						
	S	1	2										
						20	20						
						21	21						
0	S	1	5										
						Dark grayish brown (10YR4/2) loamy sand (SM)							
						22	22						
1	S	1	5										
						23 Dark gray (2.5Y4/0) sandy loam — loamy sand	23						
						24	24						
						25	25						
						26	26						

Sheet 1 of 4

JOB NO 1735

Elev. 479.2BORING NO 2

Time after drilling

## Start

Unit

**Chief,**

[illegible]



SECO Products

JOB NO 1735

LOCATION Northeast corner of building

Elev. 479.2

BORING NO 2

SOIL CONDITION While drilling 20' Time after drilling \_\_\_\_\_  
Before casing removal Depth to water \_\_\_\_\_  
After casing removal Depth to cave-in \_\_\_\_\_

Start \_\_\_\_\_  
 Unit \_\_\_\_\_  
 Chief \_\_\_\_\_

Sample No	Moisture	Blows on Sampler		Recovery	Penetration	VISUAL FIELD CLASSIFICATION AND REMARKS (intervals are in feet)	S.S. Dia 2" Weight 140 lbs Drop 30"	Pump Pressure	Boulders	Drilling fluid		Drilling Method	Graphic Log
		0/6	6/18							Fluid Type	Fluid Loss		
M						Yellowish brown (10YR5/4) Loamy sand (SM)						HSA	
					10		10						
M	1	2			11	Yellowish brown (10YR5/4) Loamy sand (SM)	11						
					12	Dark brown (10YR3/3) Silty clay loam (CL or CH)	12						
					13		13						
M	2	6			14	Brown (10YR5/3) Clay loam (CL or CH)	14						
					15		15						
M	2	7			16		16						
S					17	Dark grayish brown (10YR4/2) Loamy sand (SM)	17						
S					18	Dark grayish brown (10YR4/2) loam (SC)	18						

OF	SECO Products	
LOCATION	Northeast corner of building	Elev 479.2

JOB NO 1735  
BORING NO 2

3F UND WATER	While drilling	20'	Time after drilling	2 days	Start	
	Before casing removal		Depth to water	17'-6"	Unit	
	After casing removal		Depth to cave-in		Chief	

Sample No.	Moisture	Blows on Sampler		Recovery	Penetration	VISUAL FIELD CLASSIFICATION AND REMARKS (intervals are in feet)	S.S. Dia <u>2"</u> Weight <u>140 lbs</u> Drop <u>30'</u>	Pump Pressure	Boulders	Drilling fluid		Drilling Method	Graphic Log
		0/6	6/18							Fluid Type	Fluid Loss		
												HSA	
						Dark grayish brown (10YR4/2) Silty clay loam (CL or CH)							
	S	1	9										
						19 Dark grayish brown (10YR4/2) Loamy sand (SM) .	19						
						20	20						
	S	1	10			21 Dark yellowish brown (10YR4/4) Silty clay loam (CL or CH)	21						
						22 Dark yellowish brown (10YR4/4) Loamy sand to sand (SM)	22						
						23	23						
	S	2	8										
						24	24						
						Dark gray (2.5Y4/0) Silty clay loam (CL or CH)							
						25	25						
	S	1	4			26	26						
							27						

# FIELD BORING LOG

Sheet 4 of 4

## SECO Products

Northeast corner of building

Elev. 479.2

JOB No 1735

BORING NO 2

While drilling \_\_\_\_\_ 20'

Time after drilling

## Start.

**Before coving removal**

**Depth to water**

Unit \_

**After casing removal**

Depth to cave-in

**Chief.**

[illegible]



SECO Products

JOB NO 1735

LOCATION Northeast Corner of Lagoon

Elev. 480.3

BORING NO 3

While drilling 8.5'

Time after drilling \_\_\_\_\_

Start \_\_\_\_\_

Before casing removal \_\_\_\_\_

Depth to water \_\_\_\_\_

Unit \_\_\_\_\_

After casing removal \_\_\_\_\_

Depth to cave-in \_\_\_\_\_

Chief \_\_\_\_\_

Sample No	Moisture	Blows on Sampler		Recovery	Penetration	VISUAL FIELD CLASSIFICATION AND REMARKS (Intervals are in feet)	S.S. Dia <u>2"</u> Weight <u>140 lbs</u> Drop <u>30"</u>	Pump Pressure	Boulders	Drilling fluid		Drilling Method	Graphic Log
		0/6	6/18							Fluid Type	Fluid Loss		
1	M	2	9			Dark grayish brown (10YR4/2) Heavy silty clay loam (CL or CH)						HSA	
						1	1						
		4	13			Very dark gray (10YR3/1), Silty clay loam (CL or CH)							
						2	2						
						3	3						
2	M	8	21			Dark brown (10YR3/3) Clay loam (CL or CH)							
						4	4						
		2	6			5	5						
	M					Dark brown (10YR3/3) Very fine sandy loam (SC)							
		3	5			6	6						
						Dark brown (10YR3/3) Sandy loam (SC)							
						7	7						
		2	5			8	8						
						Dark brown (10YR3/3) Clay loam (CL or CH)							
3	S					Dark brown (10YR3/3) loamy sand (SM)							
						9	9						



JOB NO \_\_\_\_\_

BORING NO 3

SECO Products

LOCATION Northeast Corner of Lagoon

Elev. 492.8

While drilling 8.5'

Time after drilling \_\_\_\_\_

Start \_\_\_\_\_

Before casing removal \_\_\_\_\_

Depth to water \_\_\_\_\_

Unit \_\_\_\_\_

After casing removal \_\_\_\_\_

Depth to cave-in \_\_\_\_\_

Chief \_\_\_\_\_

GL JUND  
WATER

Sample No.	Moisture	Blows on Sampler		Recovery	Penetration	VISUAL FIELD CLASSIFICATION AND REMARKS (intervals are in feet)	S.S. Dia 2" Weight 140 lbs Drop 30"	Pump Pressure	Boulders	Drilling fluid		Drilling Method	Graphic Log
		0/6	6/18							Fluid Type	Fluid Loss		
S	1	3				Dark brown (10YR3/3) loamy sand (SM)						HSA	
						10 Sand lens 1" thick 10							
S	1	4				11 Dark brown (10YR3/3) loamy sand (SM)							
						12 Sand lens present 12							
S	3	10				13 Dark brown (10YR4/3) sandy clay loam (SC) 13							
S	3	12				14 Dark brown (10YR4/3) loamy sand (SM) 14							
						15 15							
S	1	4				16 Dark grayish brown (10YR4/2) and 16							
S	5	9				17 Dark brown (10YR4/3) fine-to-medium sand (SM) 17							
						18 18							

Sheet 3 of 3

JOB No 1735

BORING NO 3

Northeast Corner of Lagoon

Elev. 480.3

While drilling 8.5'

Time after drilling

## Start

**Before coving removal**

Depth to water.

Unit\_

After casing removal

**Depth to cave-in**

**Chief.**

[illegible]



SECO

JOB NO 1735

LOCATION NW Corner of Lagoon

Elev 479.2

BORING NO 4

DUND While drilling 7' Time after drilling  
 WATER Before casing removal Depth to water  
 After casing removal Depth to cave-in

Start  
 Unit  
 Chief

Moisture	Blows on Sampler		Recovery	Penetration	VISUAL FIELD CLASSIFICATION AND REMARKS (intervals are in feet)	S.S. Dia 2" Weight 140 lbs Drop 30"	Pump Pressure	Boulders	Drilling fluid		Drilling Method	Graphic Log
	0/6	6/18							Fluid Type	Fluid Loss		
M	2	6			Dark grayish brown (10YR4/2) Heavy silty clay loam (CL or CH)						HSA	
					1							
M	4	12			Dark brown (10YR3/3) Clay loam 2 (CL or CH)							
					3							
M	7	17			3							
					4							
M	2	4			5							
					6							
M	1	2			Dark brown (10YR3/3) Very fine sandy loam (SC)							
					7							
M	2	5			Dark brown (10YR3/3) Sandy loam (SC)							
					8							
S					Dark brown (10YR3/3) Clay loam (CL or CH)							
					9							
					Dark brown (10YR3/3) Loamy sand (SM)							



JOB NO \_\_\_\_\_

BORING NO 4

DI \_\_\_\_\_ SECO \_\_\_\_\_  
LOCATION NW corner of Lagoon Elev. 479.2

GL JUND \_\_\_\_\_ While drilling 7' Time after drilling \_\_\_\_\_  
WATER Before casing removal \_\_\_\_\_ Depth to water 7"-0" Start \_\_\_\_\_  
After casing removal \_\_\_\_\_ Depth to cave-in \_\_\_\_\_ Unit \_\_\_\_\_  
Chief \_\_\_\_\_

Sample No	Moisture	Blows on Sampler		Recovery	Penetration	VISUAL FIELD CLASSIFICATION AND REMARKS (intervals are in feet)	S.S. Dia <u>2"</u> Weight <u>140 lbs</u> Drop <u>30"</u>	Pump Pressure	Boulders	Drilling fluid		Drilling Method	Graphic Log
		0/6	6/18							Fluid Type	Fluid Loss		
S	1	3				Dark brown (10YR3/3) Silty clay loam (CL or CH)						HSA	
						Dark brown (10YR3/3) Loamy sand (SM)	10						
S	1	4				Dark brown (10YR3/3) Sandy clay loam (SC)	11						
						Dark brown (10YR3/3) Loamy sand (SM)							
S	2	9				Dark brown (10YR3/3) Sandy clay loam (SC)	12						
						Dark brown (10YR3/3) Loamy sand (SM)	13						
S	3	7				Dark grayish brown (10YR4/2) + Dark brown (10YR3/3) Fine to medium sand (SM)	14						
S	1	7					15						
						Grayish brown (10YR5/2) Clay loam (CL or CH)	16						
S	2	4				Dark yellowish brown (10YR4/6) Very fine to medium sand (SM)	17						
						Dark gray (2.5Y4/o) Silty clay loam (CL or CH)	18						



Sheet 1 of 4

JOB NO 1735

BORING NO 5

ION NW corner of property

Elev. 481.0

While drilling 14'

Time after drilling

## Start

**Before casing removal**

**Depth to water.**

Unit —

After casing removal

### Depth to cave-in

**Chief.**

	Moisture	Blows on Sampler		Recovery	Penetration	VISUAL FIELD CLASSIFICATION AND REMARKS (intervals are in feet)	S.S. Dia <u>2"</u> Weight <u>140 lbs</u> Drop <u>30"</u>	Pump Pressure	Boulders	Drilling fluid		Drilling Method	Graphic Log
		0/6	6/18							Fluid Type	Fluid Loss		
						Very dark grayish brown (10YR3/2) sandy clay loam (SC)						HSA	
M	2	8			1								
						Dark grayish brown (10YR4/2) clay loam (CL or CH)							
					2								
					3								
M	3	10			4								
					5								
					6								
M	2	8			7								
					8								
					9								
M	1	3				Dark brown (10YR4/3) sandy loam (SC)							

# FIELD BORING LOG

Sheet 2 of 4

## SECO Products

LOCATION Northwest corner of property

Elev 481.0

JOB NO 1735

BORING NO 5

POND WATER	While drilling <u>14'</u>	Time after drilling _____	Start _____
	Before casing removal _____	Depth to water _____	Unit _____
	After casing removal _____	Depth to cave-in _____	Chief _____

POND WATER	While drilling <u>14'</u>	Time after drilling _____	Start _____
	Before casing removal _____	Depth to water _____	Unit _____
	After casing removal _____	Depth to cave-in _____	Chief _____

Sample No.	Moisture	Blows on Sampler		Recovery	Penetration	VISUAL FIELD CLASSIFICATION AND REMARKS (intervals are in feet)	S.S. Dia Weight Drop	2" 40 lbs 30"	Pump Pressure	Boulders	Drilling fluid		Drilling Method	Graphic Log
		0/6	6/18								Fluid Type	Fluid Loss		
													HSA	
						10 Dark brown (10YR4/3) sandy loam (SC)		10						
	M	1	5			11		11						
						12 Dark brown (10YR4/3) sandy clay loam (SC)		12						
						13		13						
	M	1	5			14		14						
						15 Dark brown (10YR4/3) sandy loam (SC) lenses of heavier material		15						
	S	1	4			16		16						
						17		17						
	S					Grayish brown (10YR4/2) clay loam (CL or CH)								
								18						

Sheet 3 of 4

JOB NO 1735

Elev. 481.0BORING NO. 5

Time after drilling

**Start.**

Depth to water.

Unit\_

Depth to cove-in

Chief\_

[illegible]

Sheet 4 of 4

JOB NO \_\_\_\_\_

Elev. 481.0

BORING NO. \_\_\_\_\_

Time after drilling \_\_\_\_\_

Start 1735

Depth to water \_\_\_\_\_

Unit 5

Depth to cave-in \_\_\_\_\_

Chief \_\_\_\_\_

[illegible]

JOB NO 1735

BORING NO 6Elev. 491.8

### Depth to cave-in

Chief.

[illegible]

Sheet 2 of 5

JOB No 1735

Elev. 491.8

BORING NO 6

While drilling 23'

Time after drilling \_\_\_\_\_

Start \_\_\_\_\_

**Before coving removal**

Depth to water \_\_\_\_\_

Unit \_\_\_\_\_

After closing removal

Depth to cave-in \_\_\_\_\_

Chief \_\_\_\_\_

Sample #	Moisture	Blows on Sampler		Recovery	Penetration	VISUAL FIELD CLASSIFICATION AND REMARKS (intervals are in feet)	S.S. Dia <u>2"</u> Weight <u>40 lbs</u> Drop <u>30"</u>	Pump Pressure	Boulders	Drilling fluid		Drilling Method	Graphic Log
		0/6	6/18							Fluid Type	Fluid Loss		
						Dark grayish brown (10YR4/2)						HSA	
						and							
						10 Dark brown (10YR3/3) clay loam (CL or CH)	10						
							11						
	X	2	10				11						
							12						
							12						
							13						
						Dark grayish brown (10Yr4/2) and dark brown (10YR3/3) with some dark gray (2.5Yr4/0) clay loam (CL or CH)	13						
	M	2	9				14						
							14						
							15						
							15						
							16						
	X	2	11			Small amounts of gravel (2-5mm) mixed in	16						
							17						
							17						



# FIELD BORING LOG

Sheet 3 of 5

Client SECO Products  
LOCATION Southern Property Line Elev. 491.8

JOB NO 1735  
BORING NO 6

GROUND WATER While drilling 23' Time after drilling \_\_\_\_\_  
Before casing removal \_\_\_\_\_ Depth to water \_\_\_\_\_ Start \_\_\_\_\_  
After casing removal \_\_\_\_\_ Depth to cave-in \_\_\_\_\_ Unit \_\_\_\_\_  
Chief \_\_\_\_\_

Sample	Moisture	Blows on Sampler		Recovery	Penetration	VISUAL FIELD CLASSIFICATION AND REMARKS (intervals are in feet)	S.S. Dia <u>2"</u> Weight <u>140 lbs</u> Drop <u>30"</u>	Pump Pressure	Boulders	Drilling fluid		Drilling Method	Graphic Log
		0/6	6/18							Fluid Type	Fluid Loss		
												HSA	
M	2	11				19							
						20	Dark grayish brown (10YR4/2) (CL or CH)						
							and						
							Dark brown (10YR3/3) (CL or CH)						
M	2	7				21							
							and						
						22	Dark gray (2.5Y4/0) clay loam (CL or CH)						
						23							
S	2	8				24							
						25							
S	3	8				26	Gray (10YR5/1) and Dark Brown (10YR4/3) silty clay (CL)						



SECO Products  
LOCATION Southern Property Line Elev. 491.8

JOB NO 1735  
BORING NO 6

GROUND While drilling 23' Time after drilling \_\_\_\_\_  
WATER Before casing removal \_\_\_\_\_ Depth to water \_\_\_\_\_  
After casing removal \_\_\_\_\_ Depth to cave-in \_\_\_\_\_  
Start \_\_\_\_\_  
Unit \_\_\_\_\_  
Chief \_\_\_\_\_

Sample No	Moisture	Blows on Sampler		Recovery	Penetration	VISUAL FIELD CLASSIFICATION AND REMARKS (Intervals are in feet)	S.S. Dia <u>2"</u> Weight <u>40 lbs</u> Drop <u>30"</u>	Pump Pressure	Boulders	Drilling fluid		Drilling Method	Graphic Log
		0/6	6/18							Fluid Type	Fluid Loss		
												HSA	
						Dark brown (10YR4/3) sandy clay loam (SC)							
						28	28						
	S	2	5			Dark brown (10 YR4/3) and dark gray (2.5 Y4/0) clay loam with small amounts of (2-5mm) gravel (CL or CH)							
						29	29						
						30	30						
						31	31						
	S	2	7			Dark gray (2.5Y4/0) silty clay (CL)							
						32	32						
						33	33						
	S	1	5			34 Wood	34						
						Dark gray (2.5Y4/0) sandy loam (SC)							
						35	35						
						36	36						



SECO PRODUCTS

JOB NO 1735

LOCATION Southern Property Line

Elev.         

BORING NO 6

F IUND  
/ATER

While drilling                                  Time after drilling                                   
Before casing removal                                  Depth to water                                   
After casing removal                                  Depth to cave-in                                 

Start                                   
Unit                                   
Chief                                 

Moisture	Blows on Sampler		Recovery	Penetration	VISUAL FIELD CLASSIFICATION AND REMARKS (Intervals are in feet)	S.S. Dia <u>2"</u> Weight <u>140 lbs</u> Drop <u>30"</u>	Pump Pressure	Boulders	Drilling fluid		Drilling Method	Graphic Log
	0/6	6/18							Fluid Type	Fluid Loss		
S	1	2			same as above						HSA	
					wood							
					Dark gray (2.5Y4/0) sandy loam-loam (SC)							
					37 Dark gray (2.5Y4.0) silty clay loam (SC)	37						
					Dark gray (2.5Y4/0) silty clay loam (CL or CH)							
					38 Dark gray (2.5Y4/0) loamy sand (SM)	38						
					39	39						
					40	40						
					41	41						
					42	42						
					43	43						
					44	44						
					45	45						

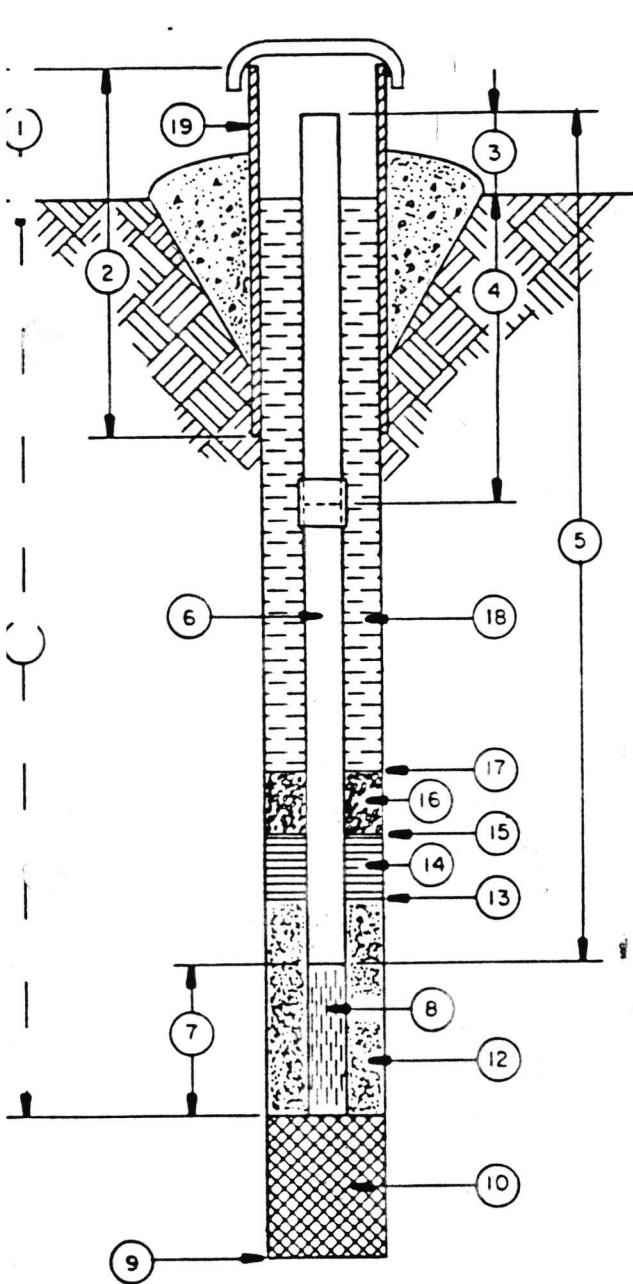
APPENDIX B

WELL CONSTRUCTION  
DETAILS

WELL CONSTRUCTION DETAILS

Job No. 1735 Boring No. 1  
Date of Installation 9/22/82 Time Started 8:00 a.m. Time Completed 3:30 p.m.  
Ground Surface Elev. 480.3

Depth measurements of well detail are from ground surface unless otherwise indicated.



- ① Height of Protective Casing Above Ground --
- ② Total Length of Protective Casing --
- ③ Height of Standpipe Above Ground 1.7'
- ④ Depth to First Coupling --  
Coupling Interval --
- ⑤ Total Length of Blank Pipe 10'
- ⑥ Type of Blank Pipe 2-1/2" Sch. 40 box thread
- ⑦ Length of Screen 15'
- ⑧ Type of Screen .006" pre-slotted
- ⑨ Total Depth of Boring 23.5' Hole Diam. 6"
- ⑩ Type of Material --
- ⑪ Depth to Bottom of Screen 23.3'
- ⑫ Type of Screen Filter medium-coarse sand  
Quantity Used --
- ⑬ Depth to Top of Filter 8'
- ⑭ Type of Seal bentonite pellets  
Quantity Used 2-1/2 gallons
- ⑮ Depth to Top of Seal 6-1/2'
- ⑯ Type of Seal Weight --  
Quantity Used --
- ⑰ Depth to Top of Seal Weight Grouted to surface
- ⑱ Type of Grout cement/bentonite  
Grout Mixture 6:1 cement/bentonite  
by volume
- ⑲ Type of Protective Casing --  
Concrete Collar Mixture --



## WELL CONSTRUCTION DETAILS

Job No. 1735

Boring No. 2

Date of Installation 9/25/82

Time Started 3:30 p.m.

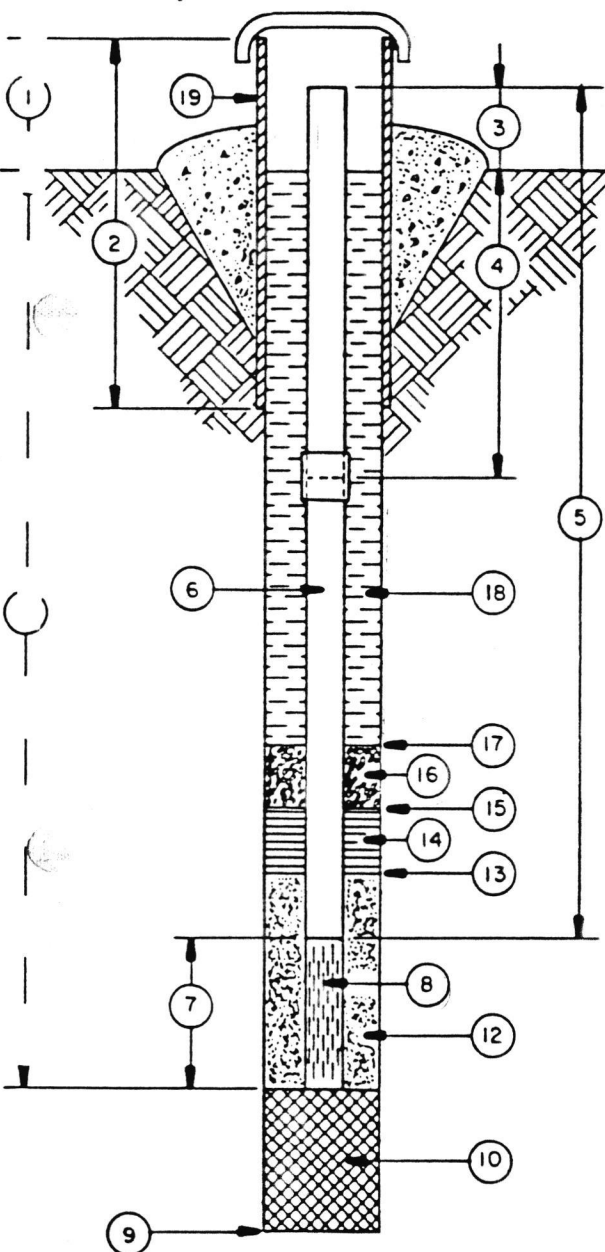
Time Completed 11:30 a.m.

Ground Surface Elev. 492.8

9/22/82

9/25/82

All depth measurements of well detail are from ground surface unless otherwise indicated.



- ① Height of Protective Casing Above Ground --
- ② Total Length of Protective Casing --
- ③ Height of Standpipe Above Ground 2.1'
- ④ Depth to First Coupling --  
Coupling Interval --
- ⑤ Total Length of Blank Pipe 20'
- ⑥ Type of Blank Pipe 2-1/2" Sch. 40 box thread
- ⑦ Length of Screen 15'
- ⑧ Type of Screen 2-1/2" Sch. 40 Box thread'
- ⑨ Total Depth of Boring 33.0' Hole Diam. 6"
- ⑩ Type of Material --
- ⑪ Depth to Bottom of Screen 32.9'
- ⑫ Type of Screen Filter Medium-coarse sand  
Quantity Used --
- ⑬ Depth to Top of Filter 16.5'
- ⑭ Type of Seal bentonite pellets  
Quantity Used 2-1/2 gallons
- ⑮ Depth to Top of Seal 13-1/2'
- ⑯ Type of Seal Weight --  
Quantity Used --
- ⑰ Depth to Top of Seal Weight Grouted to surface
- ⑱ Type of Grout Cement/bentonite  
Grout Mixture 6:1 Cement/bentonite by volume
- ⑲ Type of Protective Casing --  
Concrete Collar Mixture --

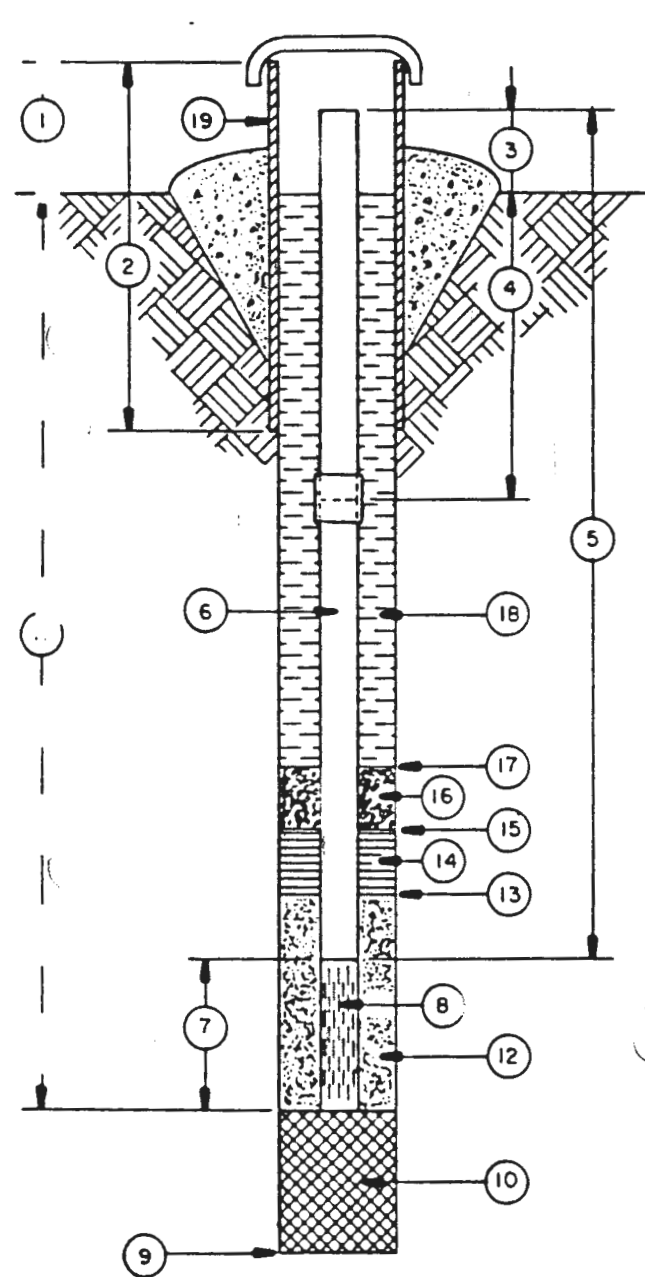
Remarks:



# WELL CONSTRUCTION DETAILS

Job No. 1735 Boring No. 3  
 Date of Installation 9/26/82 Time Started 1:00 Time Completed 9:00 a.m.  
 Ground Surface Elev. 480.3 9/25/82 9/26/82

All depth measurements of well detail are from ground surface unless otherwise indicated.



- ① Height of Protective Casing Above Ground --
- ② Total Length of Protective Casing --
- ③ Height of Standpipe Above Ground 2.5'
- ④ Depth to First Coupling --  
Coupling Interval --
- ⑤ Total Length of Blank Pipe 10'
- ⑥ Type of Blank Pipe 2-1/2" Sch. 40 Box thread
- ⑦ Length of Screen 15'
- ⑧ Type of Screen .006" pre-slotted
- ⑨ Total Depth of Boring 23.5' Hole Diam. 6"
- ⑩ Type of Material loamy sand
- ⑪ Depth to Bottom of Screen 22.5'
- ⑫ Type of Screen Filter medium-coarse sand  
Quantity Used --
- ⑬ Depth to Top of Filter 6'
- ⑭ Type of Seal bentonite pellets  
Quantity Used 2-1/2 gallons
- ⑮ Depth to Top of Seal 4'
- ⑯ Type of Seal Weight --  
Quantity Used --
- ⑰ Depth to Top of Seal Weight Grouted to surface
- ⑱ Type of Grout Cement/bentonite  
Grout Mixture 6:1 cement/bentonite by volume
- ⑲ Type of Protective Casing --  
Concrete Collar Mixture --



## WELL CONSTRUCTION DETAILS

Job No. 1735

Boring No. 4

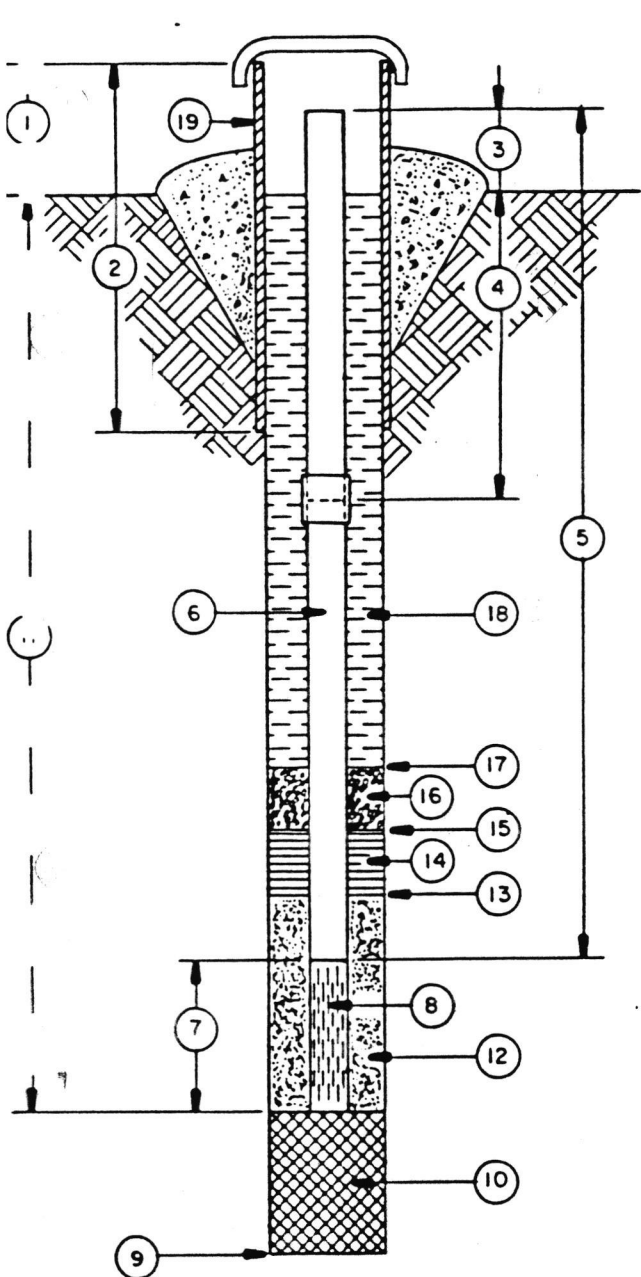
Date of Installation 9/26/82

Time Started 9:00 a.m.

Time Completed 1:30 p.m.

Ground Surface Elev. 479.2

1 Depth measurements of well detail are from ground surface unless otherwise indicated.



- ① Height of Protective Casing Above Ground --
- ② Total Length of Protective Casing --
- ③ Height of Standpipe Above Ground 2.6'
- ④ Depth to First Coupling --  
Coupling Interval --
- ⑤ Total Length of Blank Pipe 10'
- ⑥ Type of Blank Pipe 2-1/2" Sch. 40 box thread
- ⑦ Length of Screen 15"
- ⑧ Type of Screen .006" pre-slotted
- ⑨ Total Depth of Boring 22.5' Hole Diam. 6"
- ⑩ Type of Material --
- ⑪ Depth to Bottom of Screen 22.5'
- ⑫ Type of Screen Filter medium-coarse sand  
Quantity Used --
- ⑬ Depth to Top of Filter 6'
- ⑭ Type of Seal bentonite pellets  
Quantity Used 2-1/2 gallons
- ⑮ Depth to Top of Seal 3'
- ⑯ Type of Seal Weight --  
Quantity Used --
- ⑰ Depth to Top of Seal Weight Grouted to surface
- ⑱ Type of Grout Cement/bentonite  
Grout Mixture 6:1 cement/bentonite by volume  
--
- ⑲ Type of Protective Casing --  
Concrete Collar Mixture --



# WELL CONSTRUCTION DETAILS

Job No. 1735

Boring No. 5

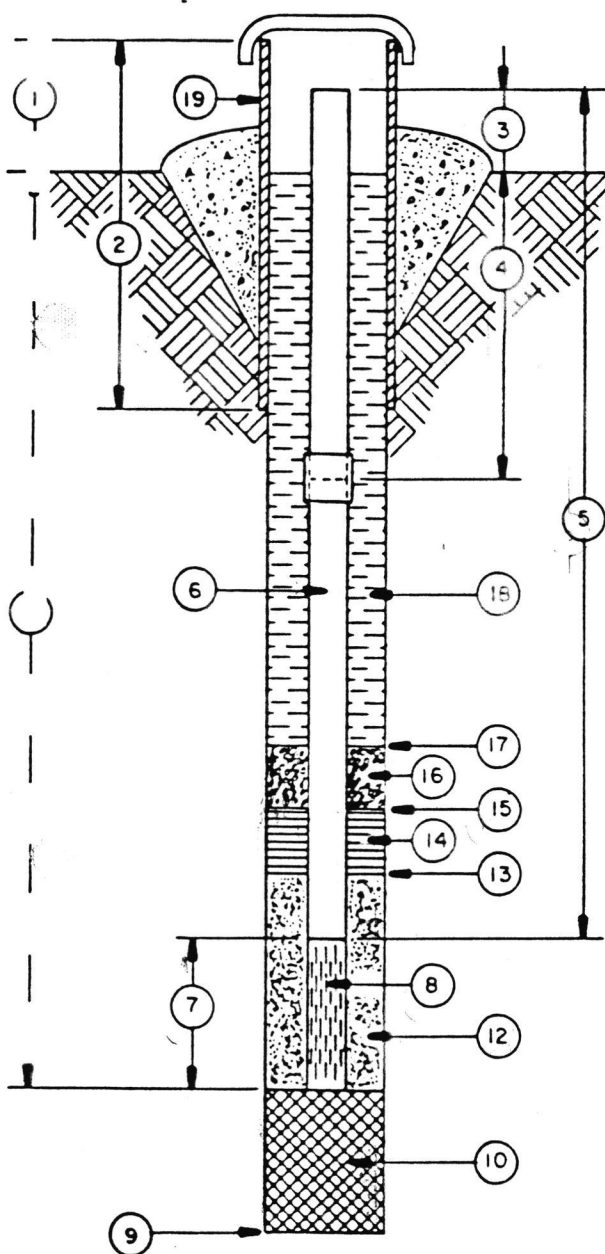
Time Started 1:30 p.m.

Time Completed 4:30 p.m.

ate of Installation 9/26/82

rc and Surface Elev. 481.0

all depth measurements of well detail are from ground surface unless otherwise indicated.



- ① Height of Protective Casing Above Ground --
- ② Total Length of Protective Casing --
- ③ Height of Standpipe Above Ground 3.2'
- ④ Depth to First Coupling --  
Coupling Interval --
- ⑤ Total Length of Blank Pipe 15'
- ⑥ Type of Blank Pipe 2-1/2" Sch. 40 box thread
- ⑦ Length of Screen 15'
- ⑧ Type of Screen .006" pre-slotted
- ⑨ Total Depth of Boring 29' Hole Diam. 6"
- ⑩ Type of Material Gravel and coarse sand
- ⑪ Depth to Bottom of Screen 26.8'
- ⑫ Type of Screen Filter medium-coarse sand  
Quantity Used --
- ⑬ Depth to Top of Filter 10'
- ⑭ Type of Seal bentonite pellets  
Quantity Used 2-1/2' gallons
- ⑮ Depth to Top of Seal 8'
- ⑯ Type of Seal Weight --  
Quantity Used --
- ⑰ Depth to Top of Seal Weight Grouted to surface
- ⑱ Type of Grout cement/bentonite  
Grout Mixture 6:1 cement/bentonite  
by volume
- ⑲ Type of Protective Casing --  
Concrete Collar Mixture --

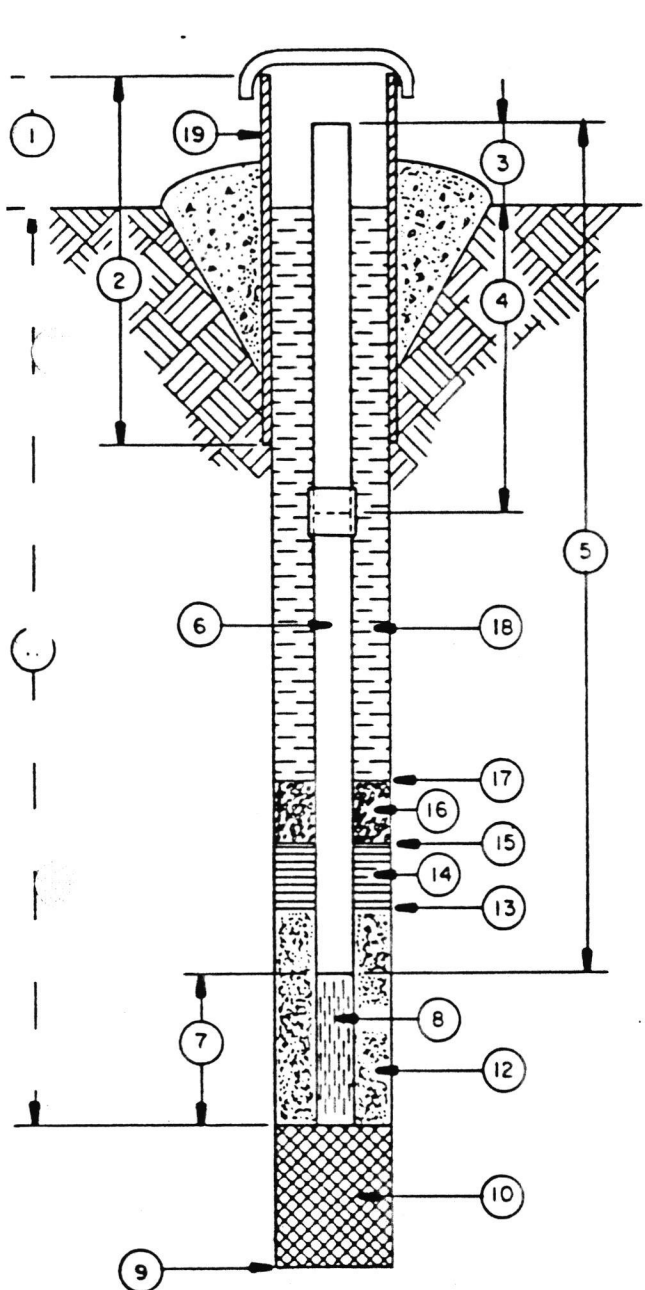
er rks:



## WELL CONSTRUCTION DETAILS

Job No. 1735 Boring No. 6  
 Date of Installation 9/27/82 Time Started 8:00 am Time Completed 2:00 pm  
 Ground Surface Elev. 491.8

All depth measurements of well detail are from ground surface unless otherwise indicated.



- ① Height of Protective Casing Above Ground 24"
- ② Total Length of Protective Casing 5'
- ③ Height of Standpipe Above Ground 1.6
- ④ Depth to First Coupling --  
Coupling Interval --
- ⑤ Total Length of Blank Pipe 25'
- ⑥ Type of Blank Pipe 2-1/2" Sch. 40 box thread
- ⑦ Length of Screen 15'
- ⑧ Type of Screen .006 pre-slotted
- ⑨ Total Depth of Boring 38.5' Hole Diam. 6"
- ⑩ Type of Material --
- ⑪ Depth to Bottom of Screen 38.4'
- ⑫ Type of Screen Filter medium coarse sand  
Quantity Used --
- ⑬ Depth to Top of Filter 14'
- ⑭ Type of Seal bentonite pellets  
Quantity Used 2-1/2 gallons
- ⑮ Depth to Top of Seal 12'
- ⑯ Type of Seal Weight --  
Quantity Used --
- ⑰ Depth to Top of Seal Weight Grouted to 2' of surface
- ⑱ Type of Grout Cement/Bentonite  
Grout Mixture 6:1 Cement/Bentonite by volume
- ⑲ Type of Protective Casing 6" black pipe  
Concrete Collar Mixture 6:1 cement/bentonite

APPENDIX C  
AQUIFER TESTING

## KEY TO APPENDIX C: AQUIFER TESTING

The diagram pictured on the aquifer testing data sheets does not depict the actual procedure used, as described in Chapter 2. A more accurate representation appears in Figure A-1. Definition of terms used on aquifer testing data sheets and Figure A-1 are as follows:

$H_0$  = height of total water level rise at time zero

$H_t$  = height of water level at measurement time  $t$

$t$  = time in minutes

$L$  = total screen length

SWL = static water level

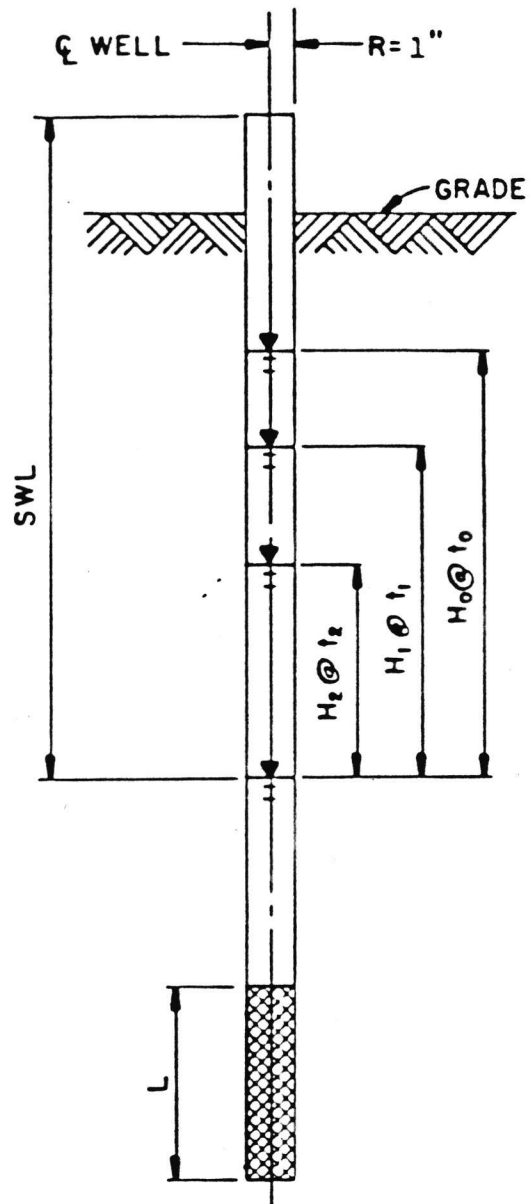


FIGURE A-1

DIAGRAM OF AQUIFER  
TESTING PROCEDURE

## AQUIER TEST RESULTS

	Depth to top of well (cm)	Depth to water table (cm)	Saturated screen length (cm)	$s$	$t$	$K$	$s$	$K$	$s$	$K$	$s$
V.E. (cm)	cm	cm	cm	-	sec	cm <sup>2</sup> /sec	cm/sec	cm/sec	cm/sec	cm/sec	cm/sec
1	710.2	350.5	359.7	$10^{-2}$	240	0.242	$6.7 \times 10^4$	0.0222	13.4	44.1	
2	1002.8	589.9	412.9	$10^{-1}$	42	1.38	$3.3 \times 10^3$	0.0133	40.1	131.2	
3	685.8	393.2	292.6	$10^{-2}$	108	0.538	$1.84 \times 10^3$	0.0156	25.8	84.7	
4	685.8	317.6	268.2	$10^{-2}$	75	0.774	$2.1 \times 10^3$	0.0303	57.32	185.0	
5	816.9	563.2	253.6	$10^{-1}$	18	3.23	$1.2 \times 10^2$	0.0199	228.1	748.2	
6	1173.5	648.0	457.2	$10^{-6}$	27	2.15	$4.7 \times 10^3$	0.0154	65.2	213.8	

$$r_e^2 = \text{radius}^2 \text{ of base hole} = 7.62^2 = 58.06 \text{ cm}^2$$

$$t = \text{time in seconds}$$

$$T = r_e^2 / t = \text{transmissivity}$$

$$S.S.L = \text{saturated screen length} = 457.2 \text{ cm maximum}$$

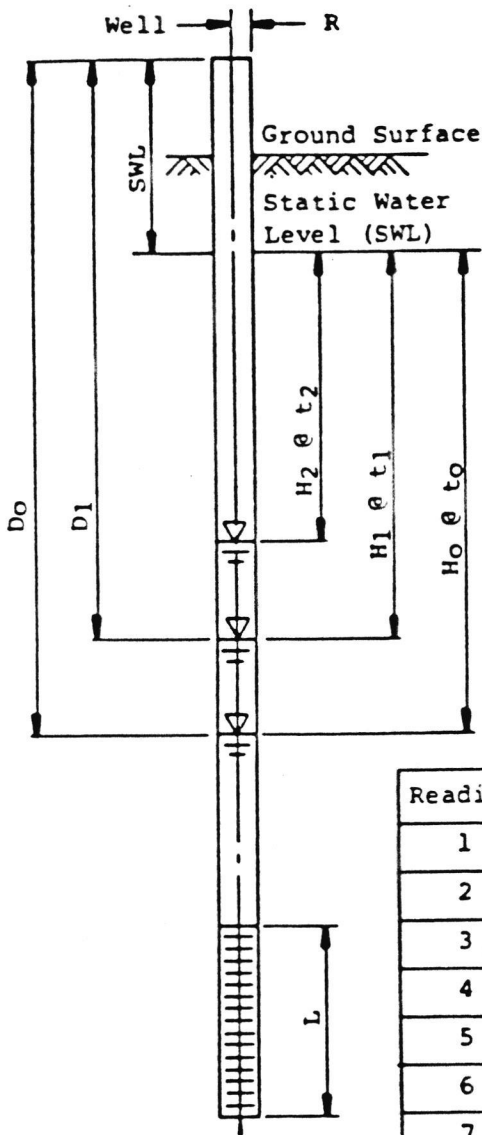
$$K = T / S.S.L = \text{coefficient of permeability}$$

$$S = \text{read from standard curves} = \text{storage coefficient}$$

$$V = K i / n = \text{Horizontal flow velocity}$$

$$n = \text{porosity, of } 35\% \text{ (from: 1975. Ward, R.C. Principles of Hydrology, 2nd Edition. McGraw Hill Book Co., England p. 191)}$$

- 1) Project SECO
- 2) Location West of Lagoon
- 3) Date 10-12-82
- 4) Personnel RRS-DTC
- 5) Well or Boring No. # 1
- 6) R=Radius of Well 1.19 (in.)
- 7) L=Length of Screen 15.0 (ft.)  
(from well detail sheet)
- 8) Static Water Level 11.5 700 (ft.)  
(depth to water)
- 9) Total Well Depth 23.625 700 (ft.)
- 10) Baildown Data (from Test) - Record  
Information in Minutes and Feet



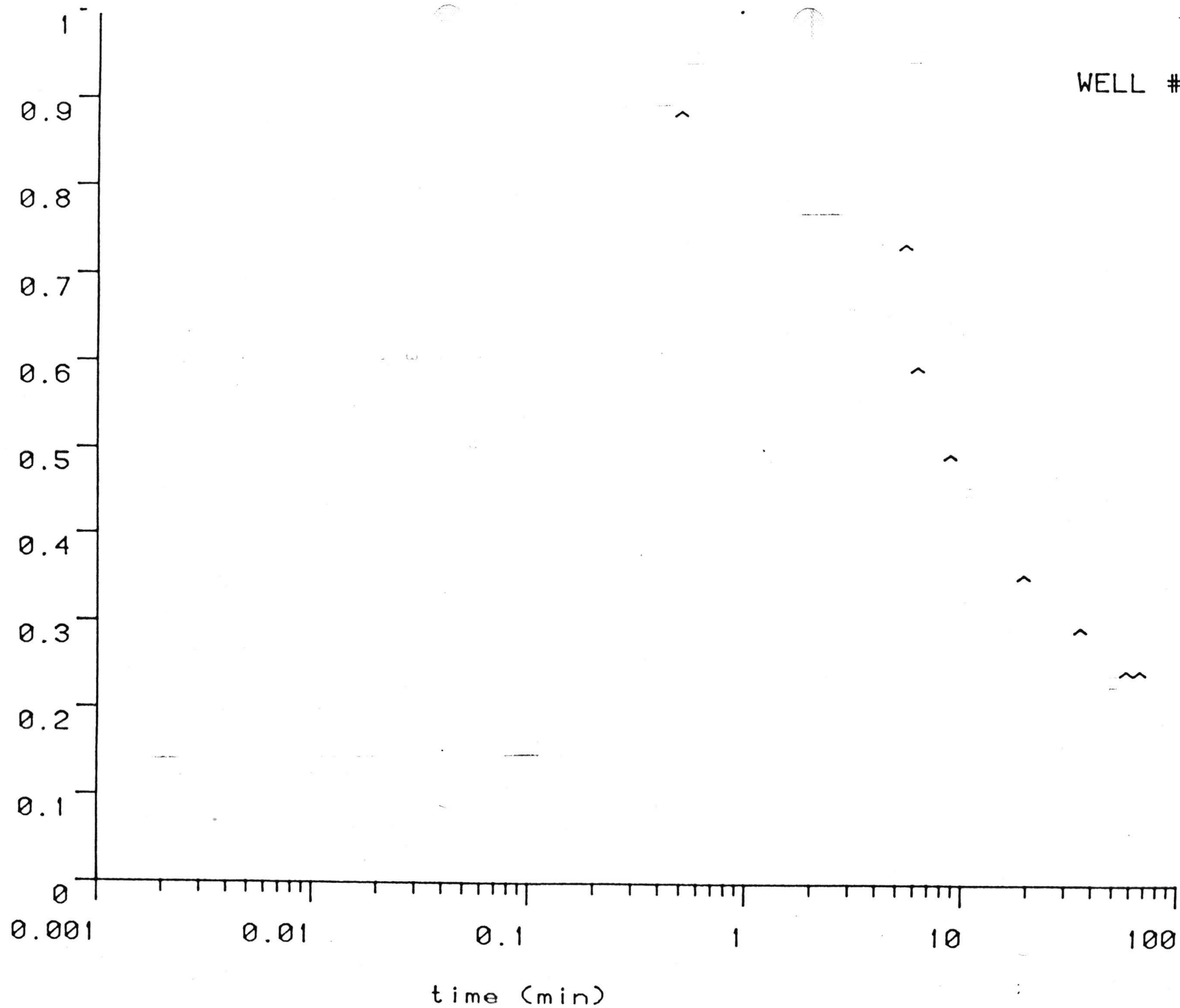
bailer slug volume:  $10' \times 1.25" = 147.26 \text{ in}^3$

Reading*	Time (Start)	Depth to Water (After Baildown) Dt (feet)	2** Dt-SWL=Ht	3** Ht/H0	
1	t0 0	D0 8.73	H0 2.77	1.00	
2 0	t1 0.50	D1 11.333	H1 0.17	0.060	1.00
3 15	t2 5.43	D2 11.354	H2 0.15	0.05	0.88
4 30	t3 6.17	D3 11.375	H3 0.125	0.04	0.73
5 45	t4 8.77	D4 11.396	H4 0.10	0.04	0.59
6 1:00	t5 19.25	D5 11.417	H5 0.083	0.03	0.49
7 1:15	t6 35.17	D6 11.437	H6 0.06	0.02	0.35
8 1:30	t7 57.50	D7 11.448	H7 0.05	0.02	0.29
9 1:45	t8 66.50	D8 11.458	H8 0.04	0.01	0.27
10 2:00	t9 189.50	D9 11.458	H9 0.04	0.01	0.24
11	t10	D10	H10		
12	t11	D11	H11		
13	t12	D12	H12		
14	t13	D13	H13		

\*Take readings until well is stabilized, if tight soils - test may be stopped prior to stabilization as necessary.

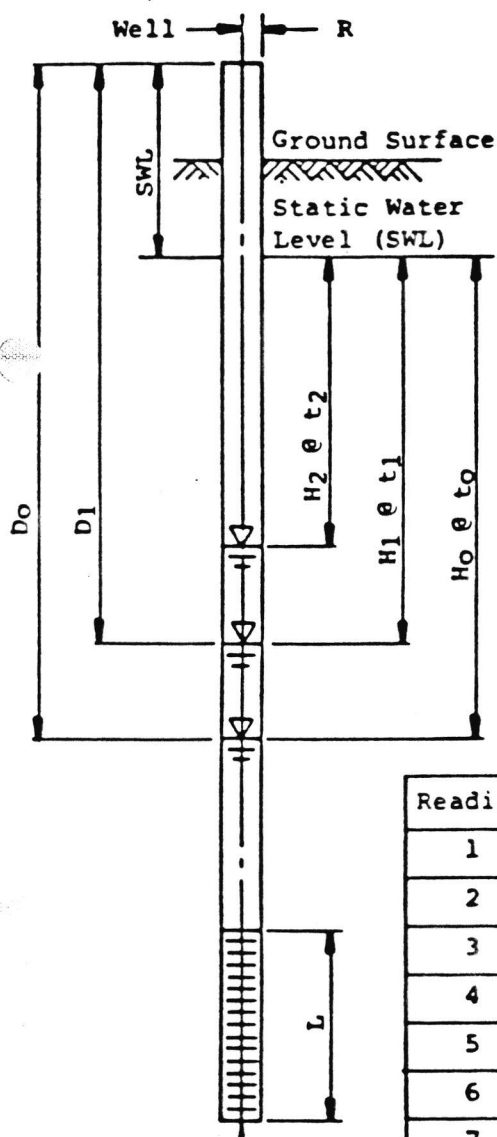
\*\*Disregard Columns 2 and 3 during baildown test. They are for office calculations.

WELL #1



- 1) Project SECO
- 2) Location far east of lagoon near plant boundary
- 3) Date 10-12-82
- 4) Personnel AAS OTC
- 5) Well or Boring No. #2
- 6) R=Radius of Well 1.187 (in.)
- 7) L=Length of Screen 15.0 (ft.)  
(from well detail sheet)
- 8) Static Water Level 19.354 TGC (ft.)  
(depth to water)
- 9) Total Well Depth 33.75 TGC (ft.)
- 10) Baildown Data (from Test) - Record  
Information in Minutes and Feet

$$\text{bailer: } 10' \times 1.25'' = 147.26 \text{ in}^3$$

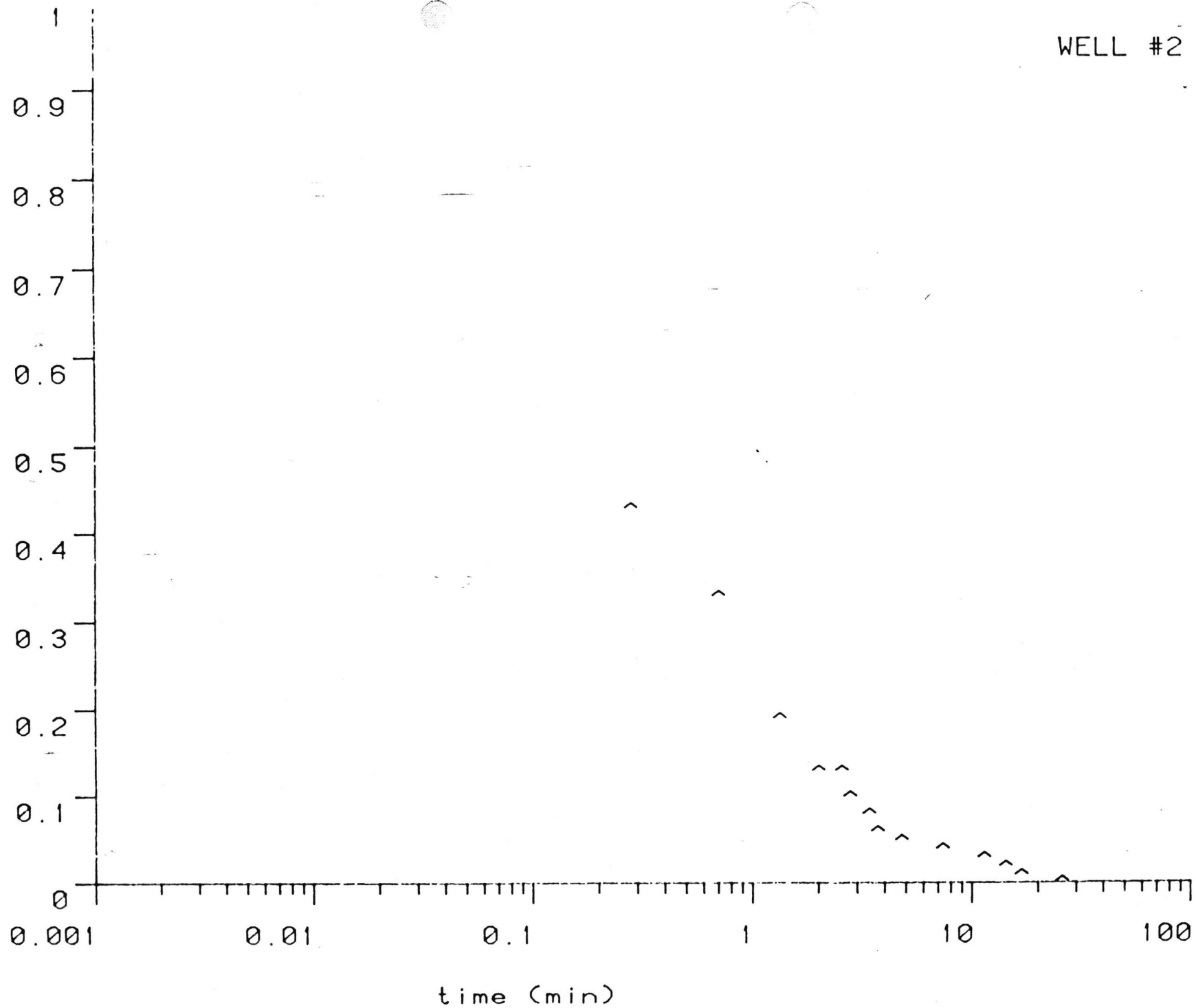


Reading*	Time (Start)	Depth to Water (After Baildown) D <sub>t</sub>	<sup>2**</sup> D <sub>t</sub> -SWL=H <sub>t</sub>	<sup>3**</sup> H <sub>t</sub> /H <sub>0</sub>
1	t <sub>0</sub> 0	D <sub>0</sub> 16.58	H <sub>0</sub> 2.77	1.00
2	t <sub>1</sub> 0.28	D <sub>1</sub> 18.17	H <sub>1</sub> 1.18	0.43
3	t <sub>2</sub> 0.70	D <sub>2</sub> 18.42	H <sub>2</sub> 0.93	0.33
4	t <sub>3</sub> 1.33	D <sub>3</sub> 18.83	H <sub>3</sub> 0.52	0.19
5	t <sub>4</sub> 2.00	D <sub>4</sub> 19.00	H <sub>4</sub> 0.35	0.13
6	t <sub>5</sub> 2.55	D <sub>5</sub> 19.04	H <sub>5</sub> 0.31	0.12
7	t <sub>6</sub> 2.78	D <sub>6</sub> 19.08	H <sub>6</sub> 0.27	0.10
8	t <sub>7</sub> 3.40	D <sub>7</sub> 19.12	H <sub>7</sub> 0.23	0.08
9	t <sub>8</sub> 3.72	D <sub>8</sub> 19.17	H <sub>8</sub> 0.18	0.06
10	t <sub>9</sub> 4.78	D <sub>9</sub> 19.21	H <sub>9</sub> 0.14	0.05
11	t <sub>10</sub> 7.35	D <sub>10</sub> 19.25	H <sub>10</sub> 0.10	0.04
12	t <sub>11</sub> 11.37	D <sub>11</sub> 19.27	H <sub>11</sub> 0.08	0.03
13	t <sub>12</sub> 14.25	D <sub>12</sub> 19.29	H <sub>12</sub> 0.06	0.02
14	t <sub>13</sub> 16.83	D <sub>13</sub> 19.31	H <sub>13</sub> 0.04	0.01
15	t <sub>14</sub> 25.83	D <sub>14</sub> 19.33	H <sub>14</sub> 0.02	0.007

\*Take readings until well is stabilized, if tight soils - test may be stopped prior to stabilization as necessary.

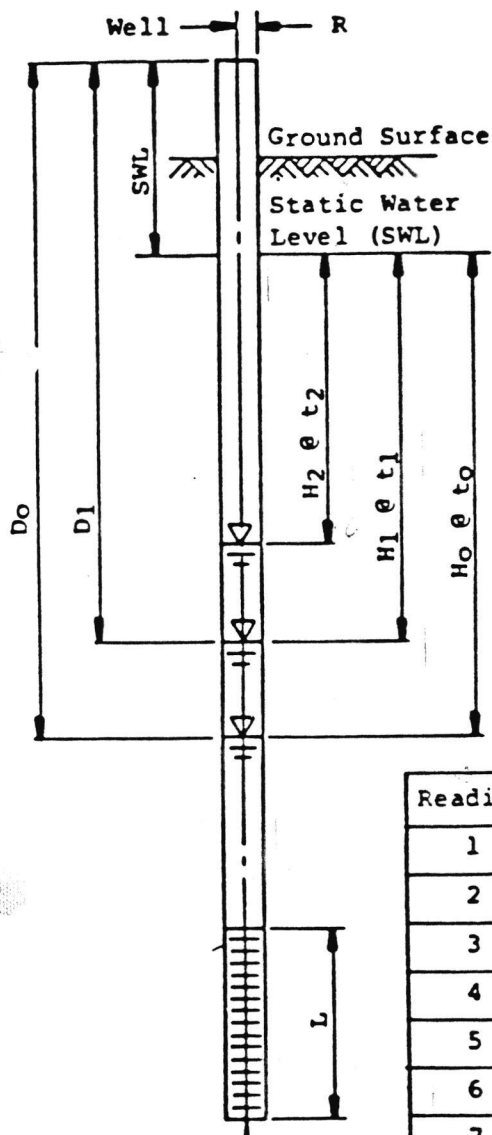
\*\*Disregard Columns 2 and 3 during baildown test. They are for office calculations.

WELL #2



- 1) Project SECO
- 2) Location northeasternmost well in bottoms area by lagoon
- 3) Date 10-12-82
- 4) Personnel RRS- DTC
- 5) Well or Boring No. #3
- 6) R=Radius of Well 1187 (in.)
- 7) L=Length of Screen 15.0 (ft.)  
(from well detail sheet)
- 8) Static Water Level 12.90 7cc (ft.)  
(depth to water)
- 9) Total Well Depth 24.75 7cc (ft.)
- 10) Baildown Data (from Test) - Record  
Information in Minutes and Feet

bailer vol: 147.26



Reading*	Time (Start)	minutes		
		Depth to Water (After Baildown) D <sub>t</sub> (ft)		
			2** D <sub>t</sub> -SWL=Ht	3** Ht/H <sub>0</sub>
1	t <sub>0</sub> 0	D <sub>0</sub> 10.13	H <sub>0</sub> 2.77	1.00
2	t <sub>1</sub> 0.38	D <sub>1</sub> 10.47	H <sub>1</sub> 2.33	0.80
3	t <sub>2</sub> 0.58	D <sub>2</sub> 10.75	H <sub>2</sub> 2.15	0.78
4	t <sub>3</sub> 0.70	D <sub>3</sub> 10.83	H <sub>3</sub> 2.07	0.75
5	t <sub>4</sub> 0.98	D <sub>4</sub> 10.92	H <sub>4</sub> 1.98	0.71
6	t <sub>5</sub> 0.98	D <sub>5</sub> 11.00	H <sub>5</sub> 1.90	0.69
7	t <sub>6</sub> 1.13	D <sub>6</sub> 11.08	H <sub>6</sub> 1.82	0.66
8	t <sub>7</sub> 1.30	D <sub>7</sub> 11.17	H <sub>7</sub> 1.73	0.62
9	t <sub>8</sub> 1.47	D <sub>8</sub> 11.25	H <sub>8</sub> 1.65	0.60
10	t <sub>9</sub> 1.67	D <sub>9</sub> 11.33	H <sub>9</sub> 1.57	0.57
11	t <sub>10</sub> 1.87	D <sub>10</sub> 11.42	H <sub>10</sub> 1.48	0.53
12	t <sub>11</sub> 2.10	D <sub>11</sub> 11.50	H <sub>11</sub> 1.40	0.50
13	t <sub>12</sub> 2.35	D <sub>12</sub> 11.58	H <sub>12</sub> 1.32	0.48
14	t <sub>13</sub> 2.72	D <sub>13</sub> 11.67	H <sub>13</sub> 1.23	0.44

\*Take readings until well is stabilized, if tight soils - test may be stopped prior to stabilization as necessary.

\*\*Disregard Columns 2 and 3 during baildown test. They are for office calculations.

BY \_\_\_\_\_ DATE \_\_\_\_\_  
CHK'D BY \_\_\_\_\_ DATE \_\_\_\_\_

# envirodyne engineers



ENVIRONMENTAL ENGINEERS  
ST. LOUIS, MO.

SHEET NO. \_\_\_\_\_ OF \_\_\_\_\_  
JOB NO. \_\_\_\_\_

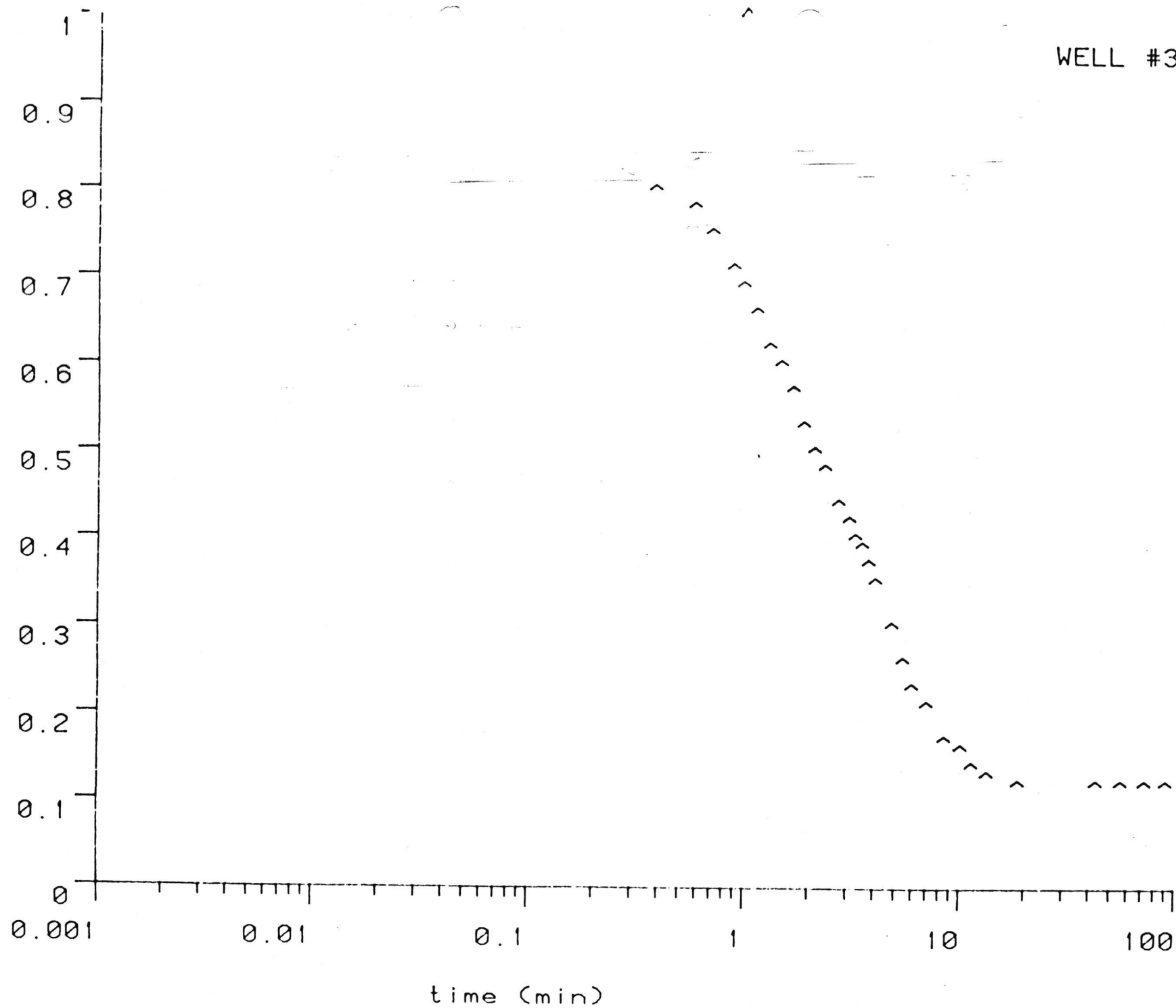
SUBJECT: \_\_\_\_\_

AQUIFER TEST DATA (CONTINUED)

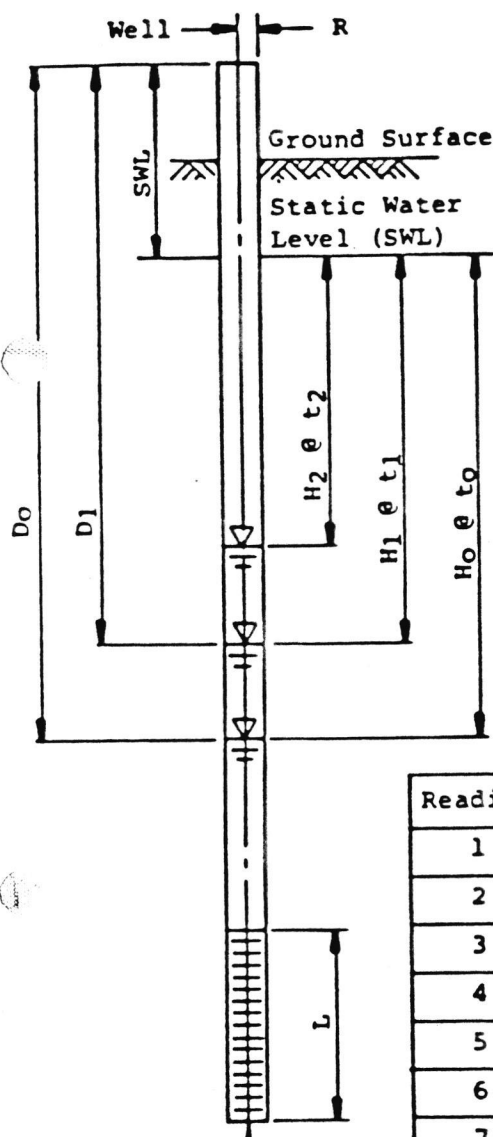
READING	TIME	D <sub>L</sub>	D <sub>L</sub> - SWL = H <sub>L</sub>	H <sub>L</sub> /H <sub>0</sub>
15	3.05	11.75	1.15	0.42
16	3.25	11.80	1.10	0.40
17	3.50	11.83	1.07	0.39
18	3.74	11.87	1.03	0.37
19	4.07	11.92	0.98	0.35
20	4.78	12.08	0.82	0.30
21	5.38	12.17	0.73	0.26
22	5.92	12.25	0.65	0.23
23	6.95	12.33	0.57	0.21
24	8.43	12.42	0.48	0.17
25	10.05	12.46	0.44	0.16
26	11.27	12.50	0.40	0.14
27	13.28	12.54	0.36	0.13
28	18.50	12.56	0.34	0.12
29	41.50	12.56	0.34	0.12
30	55.50	12.56	0.34	0.12
31	71.50	12.56	0.34	0.12
32	89.50	12.56	0.34	0.12
33				
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Boring No. #3  
Project SECO  
Date 10-12-82

WELL #3



- 1) Project SFCO
- 2) Location northwest corner of lagoon
- 3) Date 10-12-82
- 4) Personnel ARS-DTC
- 5) Well or Boring No. #4
- 6) R=Radius of Well 1.19 (in.)
- 7) L=Length of Screen 15.0 (ft.)  
(from well detail sheet)
- 8) Static Water Level 10.42 TOC (ft.)  
(depth to water)
- 9) Total Well Depth 23.83 TOC (ft.)
- 10) Baildown Data (from Test) - Record  
Information in Minutes and Feet

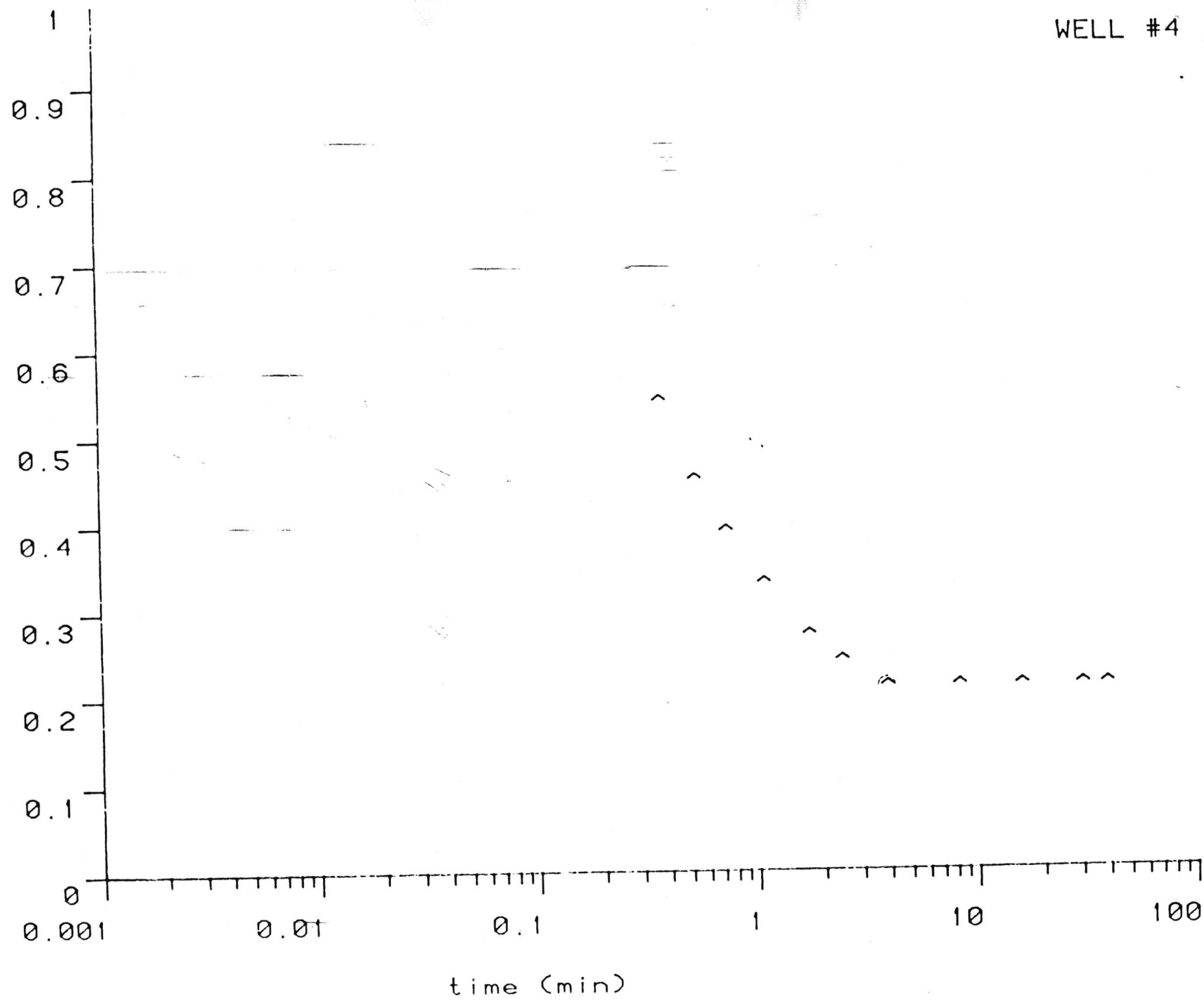


Reading*	Time (Start) minutes	Depth to Water (After Baildown) $D_t$ (ft)	$2^{**}$ $D_t - SWL = H_t$	$3^{**}$ $H_t / H_0$
1	$t_0$ 0	$D_0$ 7.65	$H_0$ 2.77	1.00
2	$t_1$ 0.37	$D_1$ 8.92	$H_1$ 1.50	0.54
3	$t_2$ 0.53	$D_2$ 9.17	$H_2$ 1.25	0.45
4	$t_3$ 0.73	$D_3$ 9.34	$H_3$ 1.08	0.39
5	$t_4$ 1.08	$D_4$ 9.50	$H_4$ 0.92	0.33
6	$t_5$ 1.72	$D_5$ 9.67	$H_5$ 0.75	0.27
7	$t_6$ 2.42	$D_6$ 9.75	$H_6$ 0.67	0.24
8	$t_7$ 3.88	$D_7$ 9.83	$H_7$ 0.59	0.21
9	$t_8$ 8.25	$D_8$ 9.83	$H_8$ 0.59	0.21
10	$t_9$ 15.83	$D_9$ 9.83	$H_9$ 0.59	0.21
11	$t_{10}$ 30.00	$D_{10}$ 9.83	$H_{10}$ 0.59	0.21
12	$t_{11}$ 39.00	$D_{11}$ 9.83	$H_{11}$ 0.59	0.21
13	$t_{12}$	$D_{12}$	$H_{12}$	
14	$t_{13}$	$D_{13}$	$H_{13}$	

\*Take readings until well is stabilized, if tight soils - test may be stopped prior to stabilization as necessary.

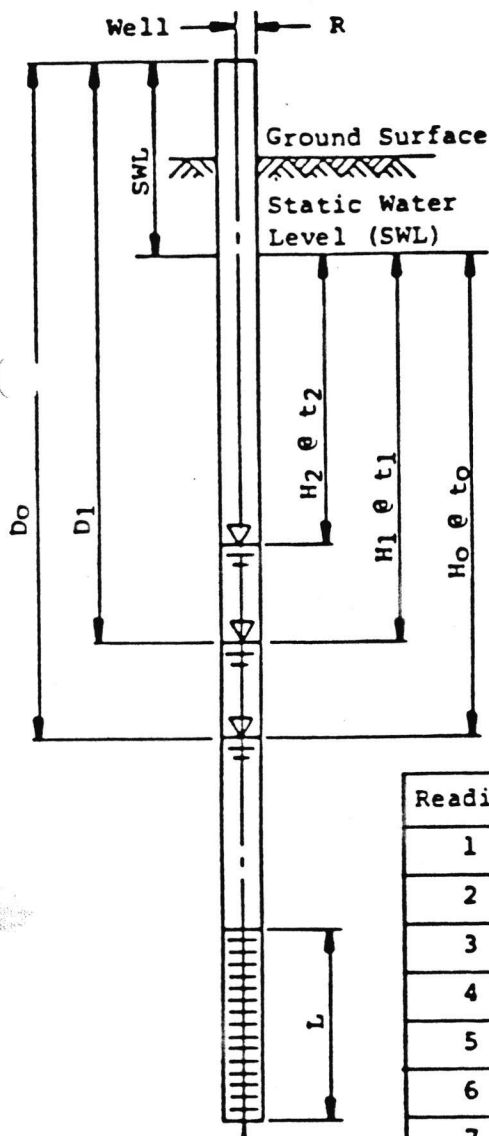
\*\*Disregard Columns 2 and 3 during baildown test. They are for office calculations.

WELL #4



- 1) Project SECO  
 2) Location West of sediment basin, near stream  
 3) Date 10-12-82  
 4) Personnel BRS-DTC

- 5) Well or Boring No. # 5  
 6) R=Radius of Well 1.19 (in.)  
 7) L=Length of Screen 15.0 (ft.)  
 (from well detail sheet)  
 8) Static Water Level 18.48 710 (ft.)  
 (depth to water)  
 9) Total Well Depth 26.34 700 (ft.)  
 10) Baildown Data (from Test) - Record  
 Information in Minutes and Feet



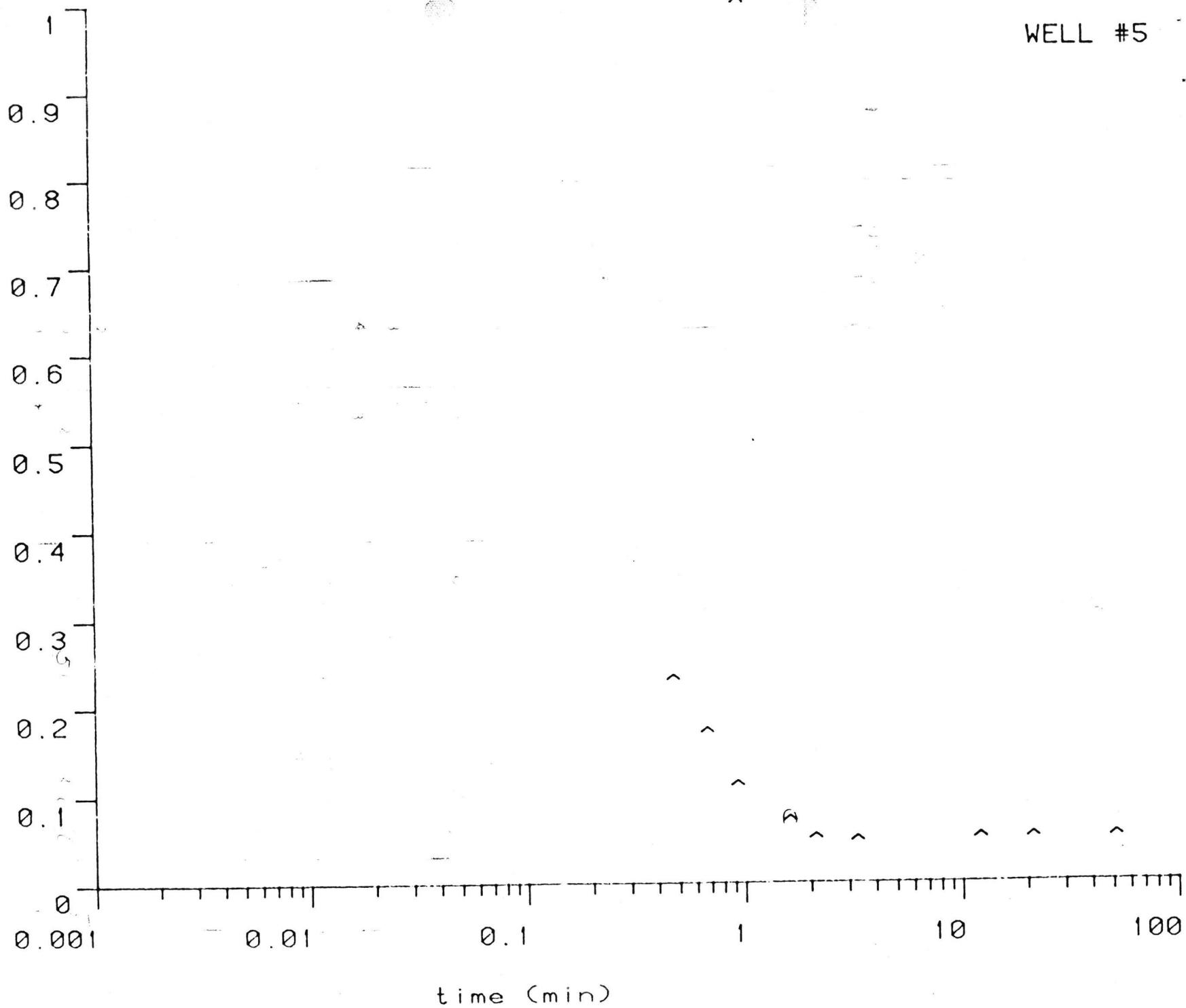
9 10

Reading*	Time (Start) minutes	Depth to Water (After Baildown) $D_t$	$\frac{2^{**}}{D_t - SWL = H_t}$	$\frac{3^{**}}{H_t / H_0}$
1	$t_0$ 0	$D_0$ 15.71	$H_0$ 2.77	1.00
2	$t_1$ 0.47	$D_1$ 17.83	$H_1$ 0.65	0.23
3	$t_2$ 0.67	$D_2$ 18.00	$H_2$ 0.48	0.17
4	$t_3$ 0.92	$D_3$ 18.17	$H_3$ 0.31	0.11
5	$t_4$ 1.60	$D_4$ 18.29	$H_4$ 0.19	0.07
6	$t_5$ 2.10	$D_5$ 18.33	$H_5$ 0.15	0.05
7	$t_6$ 3.27	$D_6$ 18.35	$H_6$ 0.13	0.047
8	$t_7$ 12.00	$D_7$ 18.35	$H_7$ 0.13	0.05
9	$t_8$ 21.00	$D_8$ 18.35	$H_8$ 0.13	0.05
10	$t_9$ 51.00	$D_9$ 18.35	$H_9$ 0.13	0.05
11	$t_{10}$	$D_{10}$	$H_{10}$	
12	$t_{11}$	$D_{11}$	$H_{11}$	
13	$t_{12}$	$D_{12}$	$H_{12}$	
14	$t_{13}$	$D_{13}$	$H_{13}$	

\*Take readings until well is stabilized, if tight soils - test may be stopped prior to stabilization as necessary.

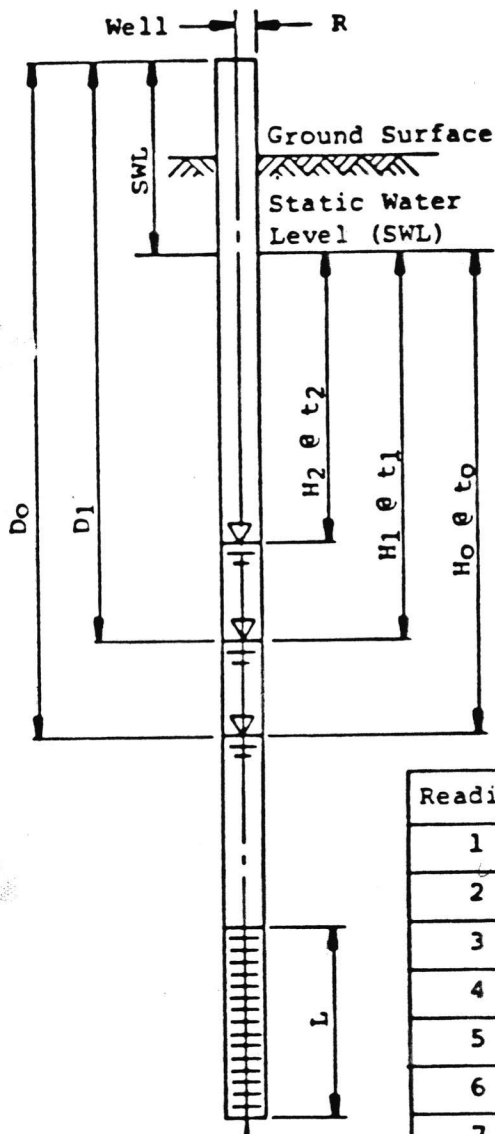
\*\*Disregard Columns 2 and 3 during baildown test. They are for office calculations.

WELL #5



- 1) Project SECO  
 2) Location Southwest corner of parking lot (background)  
 3) Date 10-12-82  
 4) Personnel RRS-DTC

- 5) Well or Boring No. #6  
 6) R=Radius of Well 1.19 (in.)  
 7) L=Length of Screen 15.0 (ft.)  
 (from well detail sheet)  
 8) Static Water Level 21.26 (ft.)  
 (depth to water)  
 9) Total Well Depth 38.58 (ft.)  
 10) Baildown Data (from Test) - Record  
 Information in Minutes and Feet

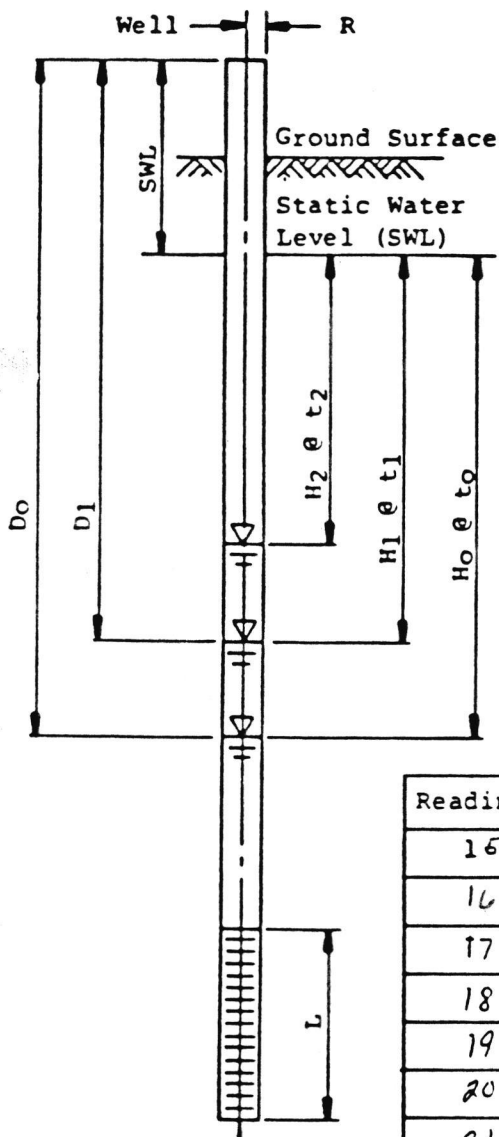


Reading*	Time (Start)	Depth to Water (After Baildown) $D_t$ (ft)	$\frac{2^{**}}{D_t - SWL = H_t}$	$\frac{3^{**}}{H_t / H_o}$
1	$t_o$ 0	$D_o$ 18.49	$H_o$ 2.77	1.00
2	$t_1$ 0.32	$D_1$ 19.08	$H_1$ 2.18	0.79
3	$t_2$ 0.47	$D_2$ 19.33	$H_2$ 1.93	0.70
4	$t_3$ 0.62	$D_3$ 19.42	$H_3$ 1.84	0.66
5	$t_4$ 0.73	$D_4$ 19.50	$H_4$ 1.76	0.63
6	$t_5$ 0.92	$D_5$ 19.75	$H_5$ 1.51	0.54
7	$t_6$ 1.15	$D_6$ 19.79	$H_6$ 1.47	0.53
8	$t_7$ 1.32	$D_7$ 19.92	$H_7$ 1.34	0.48
9	$t_8$ 1.50	$D_8$ 20.04	$H_8$ 1.22	0.44
10	$t_9$ 1.75	$D_9$ 20.17	$H_9$ 1.09	0.39
11	$t_{10}$ 1.93	$D_{10}$ 20.33	$H_{10}$ 0.93	0.33
12	$t_{11}$ 2.32	$D_{11}$ 20.42	$H_{11}$ 0.84	0.30
13	$t_{12}$ 2.65	$D_{12}$ 20.50	$H_{12}$ 0.76	0.27
14	$t_{13}$ 3.28	$D_{13}$ 20.71	$H_{13}$ 0.55	0.20

\*Take readings until well is stabilized, if tight soils - test may be stopped prior to stabilization as necessary.

\*\*\*Readings are for office calculations. They are for office calculations.

- 1) Project \_\_\_\_\_
- 2) Location \_\_\_\_\_
- 3) Date \_\_\_\_\_
- 4) Personnel \_\_\_\_\_
- 5) Well or Boring No. #16 (CONTINUED)
- 6) R=Radius of Well \_\_\_\_\_ (in.)
- 7) L=Length of Screen \_\_\_\_\_ (ft.)  
(from well detail sheet)
- 8) Static Water Level \_\_\_\_\_ (ft.)  
(depth to water)
- 9) Total Well Depth \_\_\_\_\_ (ft.)
- 10) Baildown Data (from Test) - Record  
Information in Minutes and Feet



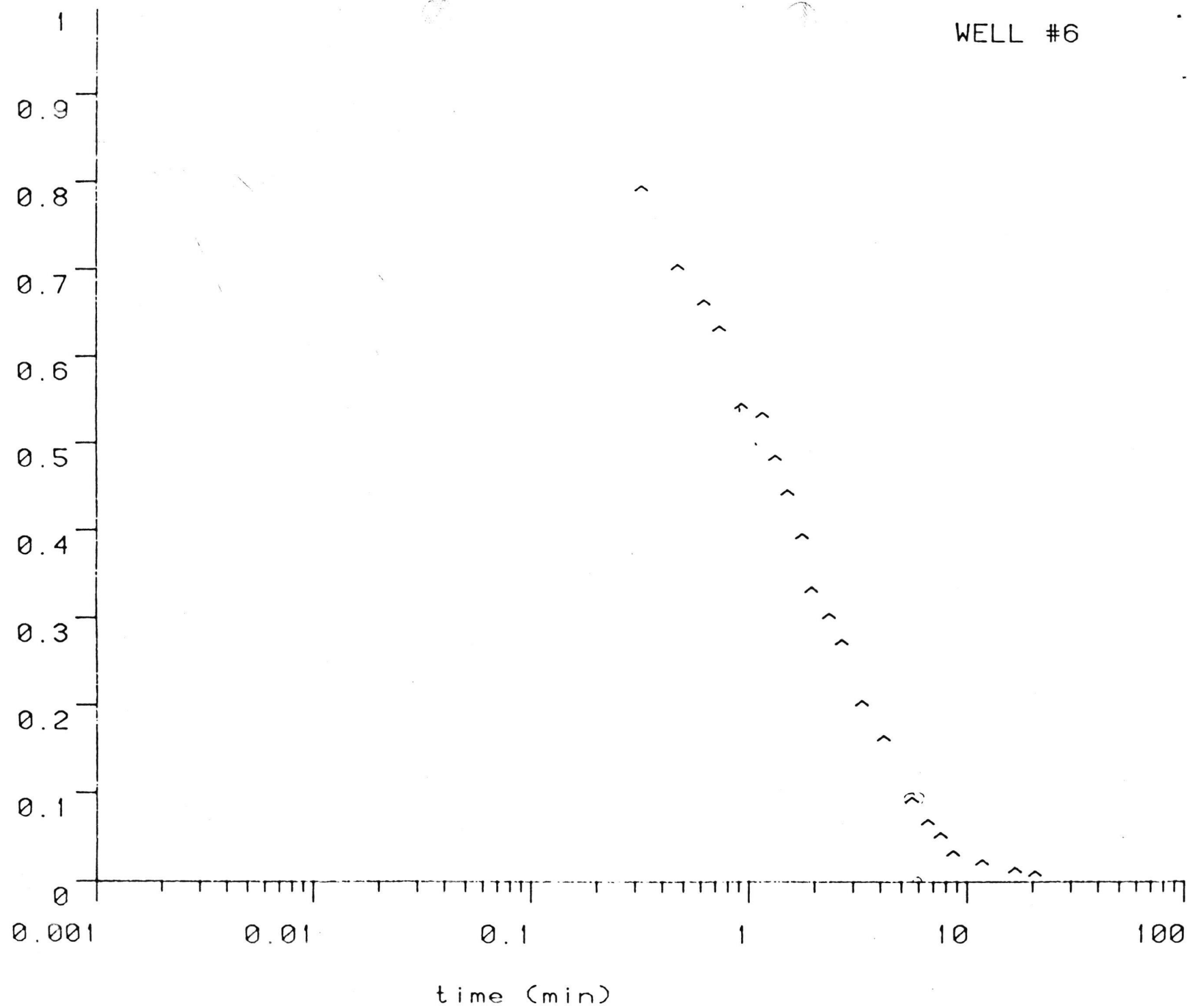
- data continued

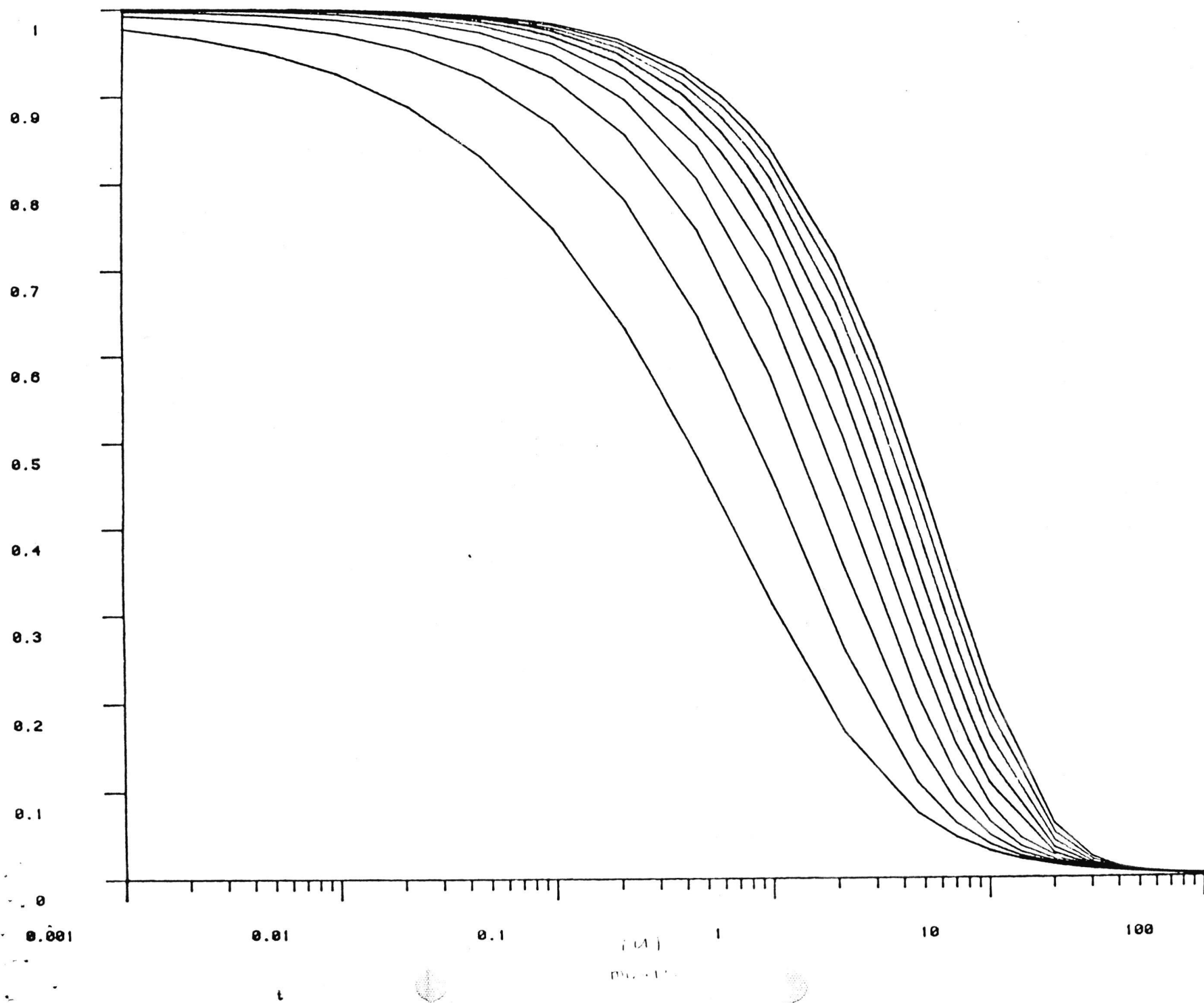
Reading*	minutes Time (Start)	Depth to Water (After Baildown) $D_t$ (ft)	$\frac{2^{**}}{D_t - SWL = H_t}$	$\frac{3^{**}}{H_t / H_0}$
15	$t_{14}$ 4.13	$D_{14}$ 20.83	$H_{14}$ 0.43	0.16
16	$t_{15}$ 5.57	$D_{15}$ 21.00	$H_{15}$ 0.26	0.09
17	$t_{16}$ 6.60	$D_{16}$ 21.08	$H_{16}$ 0.18	0.065
18	$t_{17}$ 7.55	$D_{17}$ 21.125	$H_{17}$ 0.13	0.05
19	$t_{18}$ 8.62	$D_{18}$ 21.167	$H_{18}$ 0.09	0.03
20	$t_{19}$ 11.70	$D_{19}$ 21.21	$H_{19}$ 0.05	0.02
21	$t_{20}$ 16.58	$D_{20}$ 21.23	$H_{20}$ 0.03	0.011
22	$t_{21}$ 20.50	$D_{21}$ 21.24	$H_{21}$ 0.02	0.007
-	t	D	H	
-	t	D	H	
-	t	D	H	
-	t	D	H	
-	t	D	H	
-	t	D	H	

\*Take readings until well is stabilized, if tight soils - test may be stopped prior to stabilization as necessary.

\*\*Disregard Columns 2 and 3 during baildown test. They are for office calculations.

WELL #6





## Appendix D.

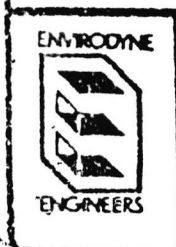
First years sampling results  
& water table elevations.

1000 C 1100 L + quarter



● MONITORING WELL  
▲ EXISTING WELL  
→ RAILROAD

Groundwater elevations  
Measured on 6-13-83  
Groundwater contours in ft



Sample Date

6/13/83

TABLE 1  
WELL DATA

<u>Well Number</u>	<u>Well Depth (Feet Below Ground Surface)</u>	<u>Top of Casing (TOC) Elevation (Feet)</u>	<u>Stick-Up (Feet)</u>	<u>Groundwater Elevation (Feet)</u>	<u>Date</u>	<u>Ground Elevation (Feet)</u>
1	23.3	482.01	1.7	473.0	6/13/83	480.3
2	32.9	494.90	2.1	479.9	6/13/83	492.8
3	22.5	482.75	2.5	474.1	6/13/83	480.3
4	22.4	481.82	2.6	473.4	6/13/83	479.2
5	26.8	484.19	3.2	470.2	6/13/83	481.0
6	38.4	493.35	1.6	474.1	6/13/83	491.8

Sample Date:

6/13/83

TABLE 2

STATISTICAL REPRESENTATION OF BACKGROUND MONITORING WELL.#2

<u>Parameter</u>	<u>Rep. 1</u>	<u>Rep. 2</u>	<u>Rep. 3</u>	<u>Rep. 4</u>	<u>Mean</u>	<u>Variance</u>
pH (units)	6.6	7.3	7.2	7.3	7.1	0.113
Specific conductance ( mhos)	575	550	575	575	568.75	156.25
TOC mg/l	42	30	39	34	36.25	28.25
TOH, $\mu\text{g/l}$ as $\text{Cl}^-$ (a)	560	870	970	910	827.5	33,492

NOTES: (a) The blank value for TOH was 530  $\mu\text{g/l}$ . The values shown are uncorrected values.

Sample Date  
6/13/83

TABLE 3  
RESULTS OF ANALYSES

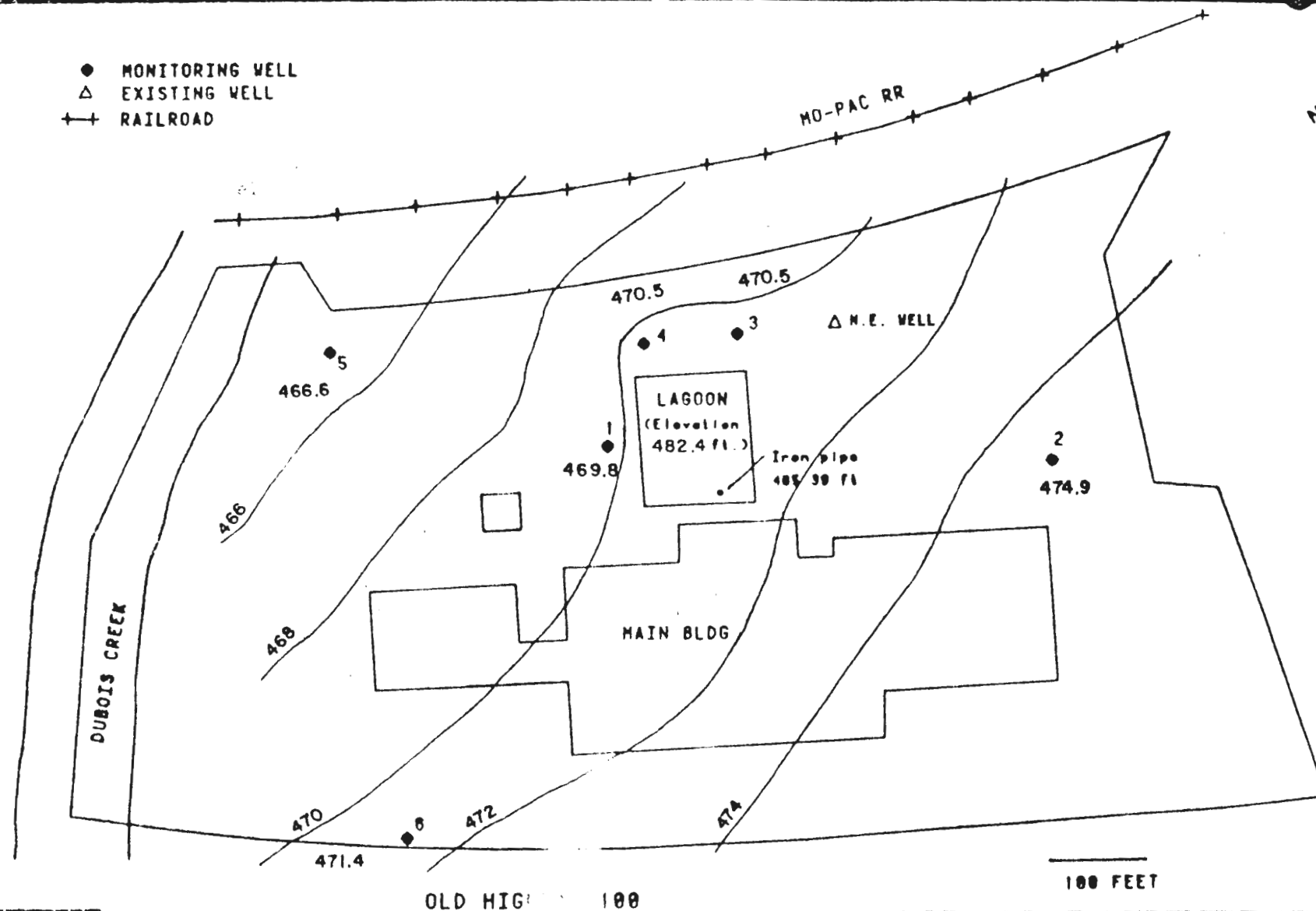
Parameters <sup>(a)</sup>	Well #1	Well #2	Well #4	Well #5
pH (units)	7.1	7.1 <sup>(b)</sup>	7.1	6.75
specific conductance (µmhos/cm)	720	575 <sup>(b)</sup>	495	475
TOC	50	36	34	30
TOH (µg/l as Cl <sup>-</sup> ) <sup>(c)</sup>	880	827 <sup>(b)</sup>	110	48
Arsenic	0.015	0.007	0.010	0.004
Barium	<0.05	<0.05	<0.05	<0.05
Cadmium	<0.001	<0.001	<0.001	<0.001
Chromium	0.004	0.004	0.001	0.003
Iron	0.16	0.12	0.07	0.07
Lead	0.002	0.001	0.001	0.001
Manganese	<0.020	0.082	<0.020	<0.020
Mercury	0.0006	0.0004	<0.0002	<0.0002
Selenium	<0.002	<0.002	<0.002	<0.002
Silver	<0.001	<0.001	<0.001	<0.001
Chloride	10.8	9.8	4.9	3.9
Cyanide	20	<5	<5	<5
Fluoride	2.12	1.45	0.56	1.26
Phenols <sup>mg/l</sup>	<0.002	<0.002	<0.002	<0.002
Sulfate	28	33	30	15
Nitrate	4.2	0.9	1.1	2.9
Fecal coliform (counts/100 ml)	<2	<2	<2	<2
Lindane (µg/l)	<0.0023	<0.0023	<0.0023	<0.0023
Endrin (µg/l)	<0.009	<0.009	<0.009	<0.009
Methoxychlor (µg/l)	<0.053	<0.053	<0.053	<0.053
Toxaphene (µg/l)	<0.333	<0.333	<0.333	<0.333
2,4-D (µg/l)	<0.076	<0.076	<0.076	<0.076
2,4,5-TP (µg/l)	<0.028	<0.028	<0.028	<0.028
Radioactive:	microcuries/liter			
Gross Alpha	<5.0	<4.0	<4.0	<4.0
Gross Beta	3.8±1.4	4.0±1.3	2.3±1.0	3.0±1.1
Radium, total	1.0±0.4	0.48±0.31	0.45±0.31	0.93±0.41

(a) Values are mg/l except as noted

(b) Value represents the mean of four replicates

(c) The blank value for TOC was 520 µg/l. The values shown are uncorrected values

- MONITORING WELL
- △ EXISTING WELL
- + RAILROAD



2 NO Quarter  
Actual Sampling Date 7-28-83  
100 FEET



Groundwater elevations  
Measured on 7-28-83  
Groundwater contours in f

FIGURE I  
SECO - MONITORING WELL LOCATIONS

Sample Date:

7/28/83

TABLE 1  
WELL DATA

<u>Well Number</u>	<u>Well Depth (Feet Below Ground Surface)</u>	<u>Top of Casing (TOC) Elevation (Feet)</u>	<u>Stick-Up (Feet)</u>	<u>Groundwater Elevation (Feet)</u>	<u>Date</u>	<u>Ground Elevation (Feet)</u>
1	23.3	482.01	1.7	469.8	7/28/83	480.3
2	32.9	494.90	2.1	474.9	7/28/83	492.8
3	22.5	482.75	2.5	470.5	7/28/83	480.3
4	22.4	481.82	2.6	470.5	7/28/83	479.2
5	26.8	484.19	3.2	466.6	7/28/83	481.0
6	38.4	493.35	1.6	471.4	7/28/83	491.8

Sample Date  
7/28/83

TABLE 2  
STATISTICAL REPRESENTATION OF BACKGROUND MONITORING WELL #2

<u>Parameter</u>	<u>Rep. 1</u>	<u>Rep. 2</u>	<u>Rep. 3</u>	<u>Rep. 4</u>	<u>Mean</u>	<u>Variance</u>
pH (units)	7.5	7.5	7.3	7.7	7.5	0.0267
Specific Conductance ( $\mu$ mhos)	613	624	619	643	624.75	168.25
TOC mg/l	24	13	24	14	18.75	36.92
TOH, $\mu$ g/l as $\text{Cl}^-$ (a)	190	34	180	47	112.75	7004.9

NOTES: (a) The blank value for TOH was 13  $\mu$ g/l. The values shown are uncorrected values.

Sample Date

7/28/83

TABLE 3  
RESULTS OF ANALYSES

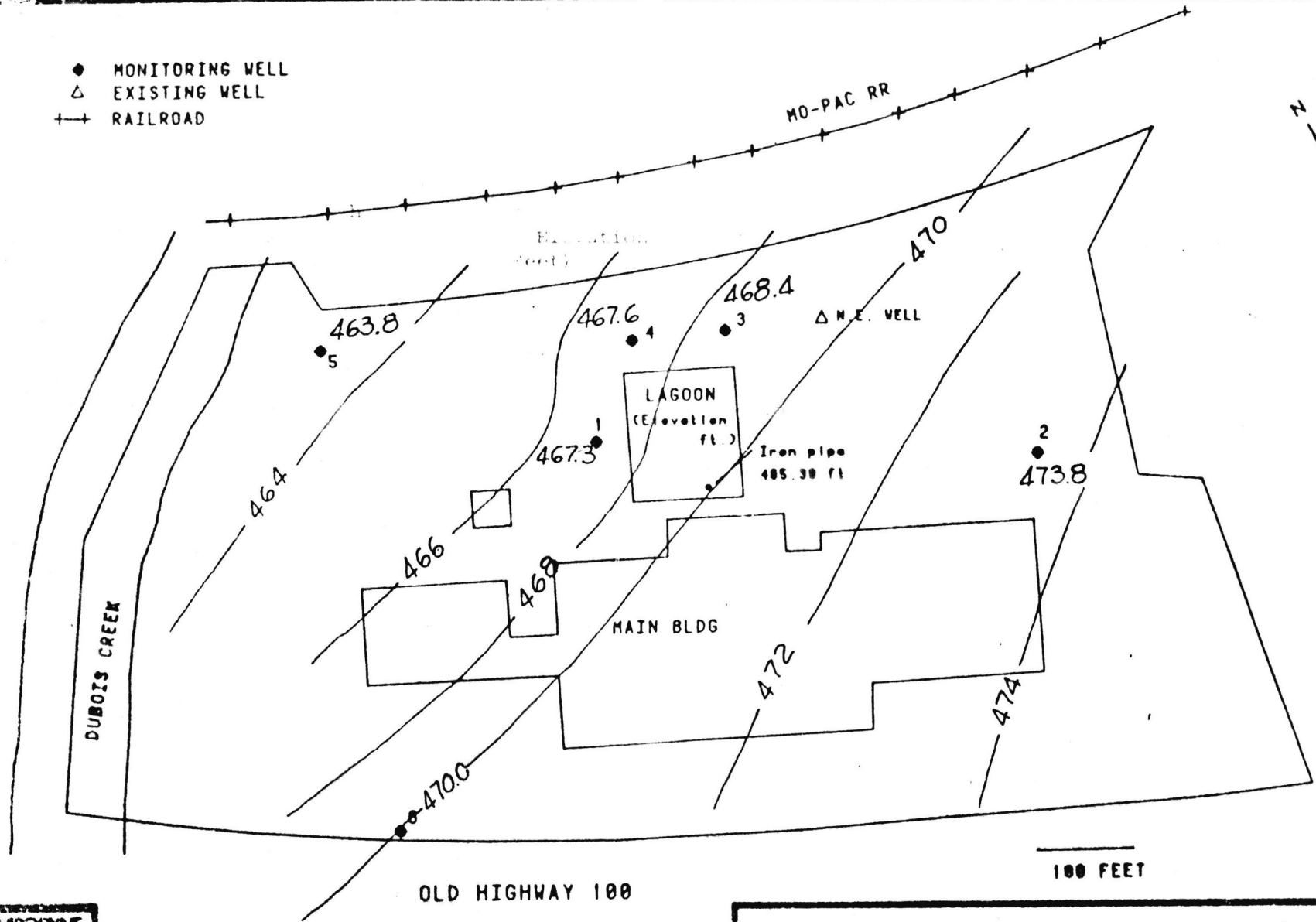
Parameters (a)	Well #1	Well #2	Well #4	Well #5
pH (units)	7.4	7.5 <sup>(b)</sup>	7.2	7.6
specific conductance ( $\mu\text{mhos/cm}$ )	822	625 <sup>(b)</sup>	510	543
TOC	28	19 <sup>(b)</sup>	15	27
TOH ( $\mu\text{g/l as Cl}^-$ ) (c)	53	113 <sup>(b)</sup>	170	4,500
Arsenic	0.005	<0.002	0.005	<0.002
Barium	<0.10	<0.10	0.14	<0.10
Cadmium	<0.001	<0.001	<0.001	<0.001
Chromium	<0.001	0.002	0.001	0.002
Iron	0.44	0.15	0.61	0.86
Lead	0.003	0.003	0.002	0.002
Manganese	0.075	0.377	0.084	<0.020
Mercury	0.2	0.2	0.5	0.2
Selenium	<0.002	<0.002	<0.002	<0.002
Silver	<0.001	<0.001	<0.001	<0.001
Chloride	21.0	9.8	3.9	6.4
Cyanide	<0.005	<0.005	<0.005	<0.005
Fluoride	1.1	1.2	0.7	
Phenols	<0.002	<0.002	<0.002	
Sulfate	230	301	178	246
Nitrate	7.7	0.45	1.05	2.35
Fecal coliform (counts/100 ml)	<2	<2	<2	<2
Lindane ( $\mu\text{g/l}$ )	<0.005	<0.005	<0.005	<0.005
Endrin ( $\mu\text{g/l}$ )	<0.005	<0.005	<0.005	<0.005
Methoxychlor ( $\mu\text{g/l}$ )	<0.005	<0.005	<0.005	<0.005
Toxaphene ( $\mu\text{g/l}$ )	<0.05	<0.05	<0.05	<0.05
2,4-D ( $\mu\text{g/l}$ )	<0.05	<0.05	<0.05	<0.05
2,4,5-TP ( $\mu\text{g/l}$ )	<0.005	<0.005	<0.005	<0.005
Radioactive:				
Gross Alpha	3.0 $\pm$ 2	5.0 $\pm$ 4	<2	25 $\pm$ 11
Gross Beta	9.0 $\pm$ 2	13 $\pm$ 3	7.0 $\pm$ 2	24 $\pm$ 3
Radium, total	<1	4.0 $\pm$ 1	3.0 $\pm$ 1	8.0 $\pm$ 1

(a) Values are mg/l except as noted

(b) Value represents the mean of four replicates

(c) Blank value for TOH was 11  $\mu\text{g/l}$ . The values shown are uncorrected values.

- ◆ MONITORING WELL
- △ EXISTING WELL
- + RAILROAD



3RD Quarter  
 Actual Sampling date 8-18-83  
 100 FEET

100 FEET

OLD HIGHWAY 100

Groundwater elevations  
 Measured on 8-18-83  
 Groundwater contours in ft

SECO - MONITORING WELL LOCATIONS  
 AND WATER TABLE MAP



Sample Date:

8/18/83

TABLE 1  
WELL DATA

<u>Well Number</u>	<u>Well Depth (Feet Below Ground Surface)</u>	<u>Top of Casing (TOC) Elevation (Feet)</u>	<u>Stick-Up (Feet)</u>	<u>Groundwater Elevation (Feet)</u>	<u>Date</u>	<u>Ground Elevation (Feet)</u>
1	23.3	482.01	1.7	467.3	8/18/83	480.3
2	32.9	494.90	2.1	473.8	8/18/83	492.8
3	22.5	482.75	2.5	468.4	8/18/83	480.3
4	22.4	481.82	2.6	467.6	8/18/83	479.2
5	26.8	484.19	3.2	463.8	8/18/83	481.0
6	38.4	493.35	1.6	470.0	8/18/83	491.8

Sample Date  
8/18/83

TABLE 2

STATISTICAL REPRESENTATION OF BACKGROUND MONITORING WELL #2

<u>Parameter</u>	<u>Rep. 1</u>	<u>Rep. 2</u>	<u>Rep. 3</u>	<u>Rep. 4</u>	<u>Mean</u>	<u>Variance</u>
pH (units)	6.6	6.2	6.4	6.5	6.4	0.0292
Specific conductance ( mhos)	600	700	600	625	631	2,239
TOC mg/l	72	76	84	82	78.5	30.33
TOH, µg/l as Cl <sup>-</sup> (a)	560	1,700	590	1,500	1,087	357,025

NOTES: (a) The blank value for TOH was µg/l. The values shown are uncorrected values.

Less Than 5 mg/l.

Sample Date  
8/18/83

TABLE 3  
RESULTS OF ANALYSES

Parameters (a)	Well #1	Well #2	Well #4	Well #5
pH (units)	6.4	6.4 <sup>(b)</sup>	6.2	6.4
specific conductance (µmhos/cm)	800	631 <sup>(b)</sup>	550	500
TOC	24108	-78	1258	1270
TOH (µg/l as Cl <sup>-</sup> ) <sup>(c)</sup>	35	-1,087	9,700	140
Arsenic	<0.002	<0.002	<0.004	<0.002
Barium	<0.1	<0.1	<0.1	<0.1
Cadmium	<0.001	<0.001	<0.001	<0.001
Chromium	<0.04	<0.04	<0.04	<0.04
Iron	0.150	0.086	0.744	0.230
Lead	<0.002	<0.002	0.006	0.002
Manganese	0.095	0.426	0.082	0.089
Mercury	0.0005	0.0004	0.0004	0.0004
Selenium	<0.002	<0.002	<0.002	<0.002
Silver	<0.001	<0.001	<0.001	<0.001
Chloride	20	7.8	3.5	3.4
Cyanide	<0.005	<0.005	<0.005	<0.005
Fluoride	1.23	0.35	0.81	0.60
Phenols	<0.002	<0.002	<0.002	<0.002
Sulfate (as SO <sub>4</sub> )	25	43	18	<5
Nitrate (as N)	6.5	0.4	1.0	3.1
Fecal coliform (counts/100 ml)	<5	<5	45	<5
Lindane (µg/l)	<0.002	<0.002	<0.002	<0.002
Endrin (µg/l)	<0.003	<0.003	<0.003	<0.003
Methoxychlor (µg/l)	<0.006	<0.006	<0.006	<0.006
Toxaphene (µg/l)	<0.04	<0.04	<0.04	<0.04
2,4-D (µg/l)	<0.01	<0.01	<0.01	<0.01
2,4,5-TP (µg/l)	<0.003	<0.003	<0.003	<0.003
Radioactive:				
Gross Alpha	20±12	26±13	29±13	17±12
Gross Beta	32±3	32±3	42±3	18±3
Radium, total	6±1	7±1	4±1	4±1

(a) Values are mg/l except as noted

(b) Value represents the mean of four replicates

(c) The blank value for TOH was 5 µg/l. The values shown are uncorrected values



ENVIRODYNE  
ENGINEERS

January 4, 1984  
1971

JAN 26 1984

WASTE  
MANAGEMENT PROGRAM

Mr. Larry Colvin  
SECO Products  
Post Office Box 187  
Washington, MO 63090

Dear Larry:

As described in my letter to you dated November 30, 1983, we discovered an error in our sampling procedure which we believed may have been the cause of the generally high reported values for TOH. We resampled the monitoring wells again on November 22, 1983, specifically for TOH, but used a corrected sampling procedure. The TOH results from these samples confirmed our suspicions.

The initial values of TOH reported for samples collected October 4, 1982 were correct. All TOH data for samples collected June 13, July 28 and August 18, 1983, are invalid. The TOH data reported in the enclosed tables are valid, and come from samples collected on November 22, 1983 rather than from the samples collected on October 28, 1983. The TOH data for samples collected on October 28, 1983 are invalid, and, therefore, are not included in this data report. On our next invoice we will credit you for the three sets of invalid TOH data at the rate of \$37.50 per sample. This amounts to a total credit of \$787.50.

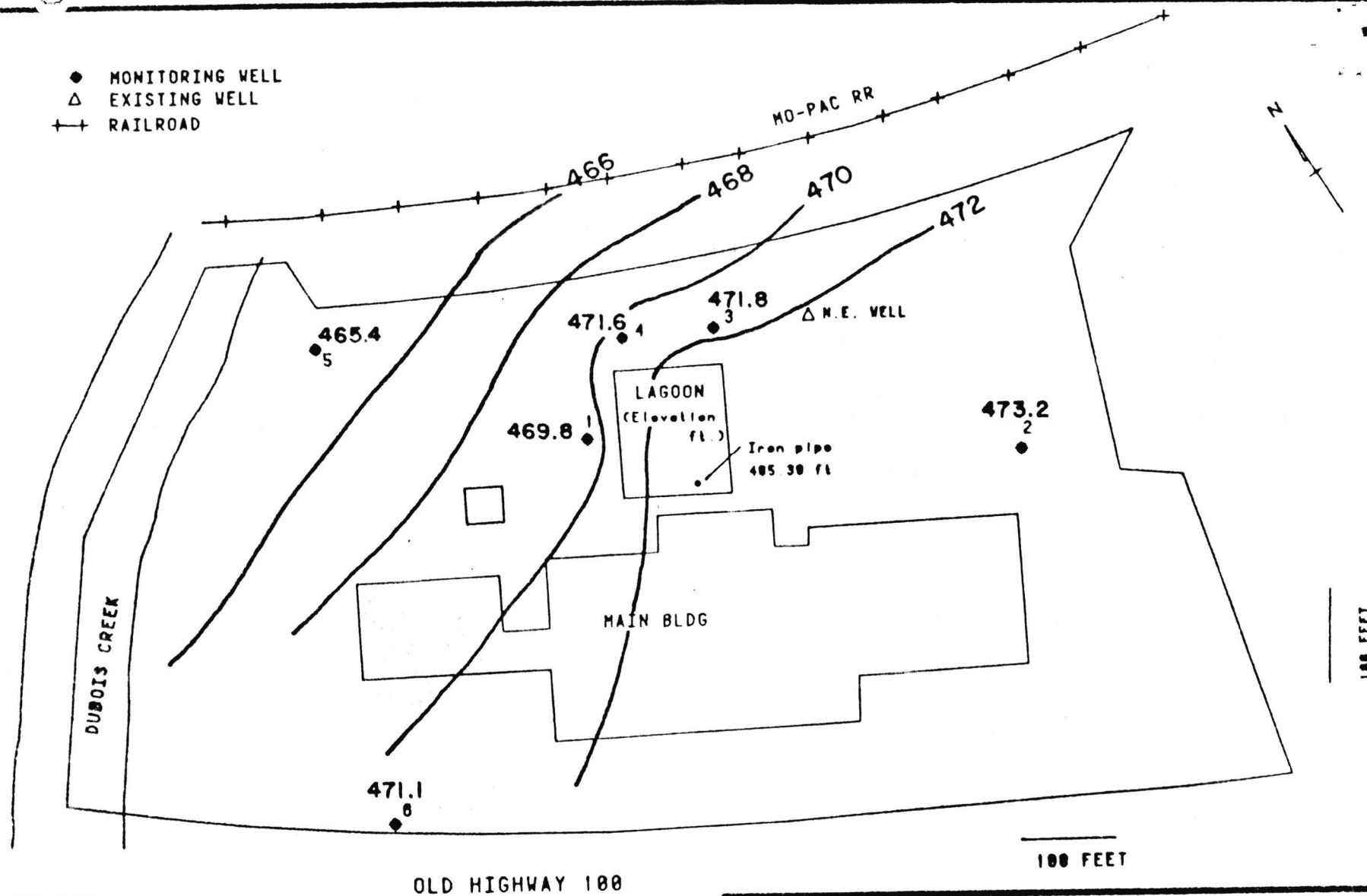
I hope this error has not caused you any inconvenience. If you have any questions, please feel free to call.

Sincerely,

Donald R. Monnot  
Senior Hydrogeologist

DRM/csg  
Enclosures

- MONITORING WELL
- △ EXISTING WELL
- + RAILROAD



Groundwater elevations  
Measured on 11-22-83  
Groundwater contours in ft

FIGURE 1  
SECO - MONITORING WELL LOCATIONS

Sample Dates:

10/28/83 & 11/22/83

TABLE 1  
WELL DATA

<u>Well Number</u>	<u>Well Depth (Feet Below Ground Surface)</u>	<u>Top of Casing (TOC) Elevation (Feet)</u>	<u>Stick-Up (Feet)</u>	<u>Groundwater Elevation (Feet)</u>	<u>Date</u>	<u>Ground Elevation (Feet)</u>
1	23.3	482.01	1.7	469.8	11/22/83	480.3
2	32.9	494.90	2.1	473.2	11/22/83	492.8
3	22.5	482.75	2.5	471.8	11/22/83	480.3
4	22.4	481.82	2.6	471.6	11/22/83	479.2
5	26.8	484.19	3.2	465.4	11/22/83	481.0
6	38.4	493.35	1.6	471.1	11/22/83	491.8

Sample Dates  
10/28/83 + 11/22/83

TABLE 2

STATISTICAL REPRESENTATION OF BACKGROUND MONITORING WELL #2

<u>Parameter</u>	<u>Rep. 1</u>	<u>Rep. 2</u>	<u>Rep. 3</u>	<u>Rep. 4</u>	<u>Mean</u>	<u>Variance</u>
pH (units)	7.8	7.8	7.85	7.6	7.76	0.009
Specific conductance ( mhos)	780	796	815	841	808	516.5
TOC mg/l	76	70.3	69.3	69.9	71.4	9.67
TOH, µg/l as Cl <sup>-</sup> (a)	6 <sup>a</sup>	<5 <sup>a</sup>	6 <sup>a</sup>	7 <sup>a</sup>	6 <sup>a</sup>	0.667

Notes: <sup>a</sup> Samples collected 11/22/83  
If not otherwise noted, samples were collected on 10/28/83

10/28/83 + 11/22/83

TABLE 3  
RESULTS OF ANALYSES<sup>b</sup>

Parameters (a)	Well #1	Well #2	Well #4	Well #5
pH (units)	7.2	7.76 <sup>c</sup>	7.0	7.75
specific conductance (µmhos/cm)	911	808 <sup>c</sup>	571	593
TOC	93.5	71.4 <sup>c</sup>	69.3	61.3
TOH (µg/l as Cl <sup>-</sup> ) (d)	39	6 <sup>c</sup>	38	130
Arsenic	0.016	<0.002	0.020	0.005
Barium	<0.1	<0.1	<0.1	<0.1
Cadmium	<0.001	<0.001	<0.001	<0.001
Chromium	0.005	<0.002	0.004	0.002
Iron	0.06	<0.04	<0.05	0.06
Lead	<0.002	<0.002	<0.002	<0.002
Manganese	0.10	0.09	0.04	<0.02
Mercury (µg/l)	<0.2	<0.2	<0.2	<0.2
Selenium	<0.002	<0.002	<0.002	<0.002
Silver	<0.001	<0.001	<0.001	<0.001
Chloride	27	7.0	4.4	6.4
Cyanide	<0.005	<0.005	<0.005	<0.005
Fluoride	1.14	0.37	0.67	0.64
Phenols	<0.002	<0.002	<0.002	<0.002
Sulfate	30.0	52.5	35.0	30.0
Nitrate	8.2	0.7	3.8	3.8
Fecal coliform (counts/100 ml)	<10	<5	<5	<5
Lindane (µg/l)	<0.01	<0.01	<0.01	<0.01
Endrin (µg/l)	<0.03	<0.03	<0.03	<0.03
Methoxychlor (µg/l)	<0.5	<0.5	<0.5	<0.5
Toxaphene (µg/l)	<0.5	<0.5	<0.5	<0.5
2,4-D (µg/l)	<0.01	<0.01	<0.01	<0.01
2,4,5-TP (µg/l)	<0.01	<0.01	<0.01	<0.01
Radioactive:				
Gross Alpha (pCi/l)	<2	<2	<2	11+6
Gross Beta (pCi/l)	4+2	<3	4+2	10+2
Radium, total (pCi/l)	3+1	2+1	2+1	3+1

(a) Values are mg/l except as noted

(b) Samples collected on 10/28/83, except as noted.

(c) Represents the mean shown on Table 2.

(d) Samples collected on 11/22/83.

# Seco Products

A Member of Bastian Industries

Seco Products  
P.O. Box 187  
Old Hwy 100 East  
Washington, MO 63090

JANUARY 9, 1984

UNITED STATES ENVIRONMENTAL PROTECTION AGENCY  
REGION VII  
324 EAST ELEVENTH STREET  
KANSAS CITY, MISSOURI 64106

ATTENTION: MR. DON SANDIFER

DEAR MR. SANDIFER:


ENCLOSED IS OUR LATEST GROUND WATER MONITORING REPORT FOR 10/28/83. PLEASE NOTE THAT THE TOH RESULTS IN THIS REPORT ARE FROM THE 11/22/83 SAMPLING. THE TOH SAMPLINGS TAKEN 10/28/83 WERE INCORRECTLY TAKEN.

ALSO, ENVIRODYNE ENGINEERS HAS ADVISED US THAT THE OCTOBER 4, 1982 TOH SAMPLINGS WERE CORRECT WHEREAS THE JUNE 13, JULY 28 AND AUGUST 18, 1983 SAMPLINGS WERE INVALID.

THIS SAMPLING ERROR SEEMS TO BE THE PROBLEM WITH RECEIVING HIGH TOH READINGS. I WILL CALL YOU LATER THIS WEEK SO WE CAN DISCUSS RE-SAMPLING OR WHATEVER MEANS THE EPA REQUIRE TO RESOLVE THIS UNFORTUNATE SITUATION.

SINCERELY,

SECO PRODUCTS



LARRY COLVIN  
PLANT ENGINEERING COORDINATOR

LC/SS

ENC.